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Preliminary layout report

Kupres wind farm

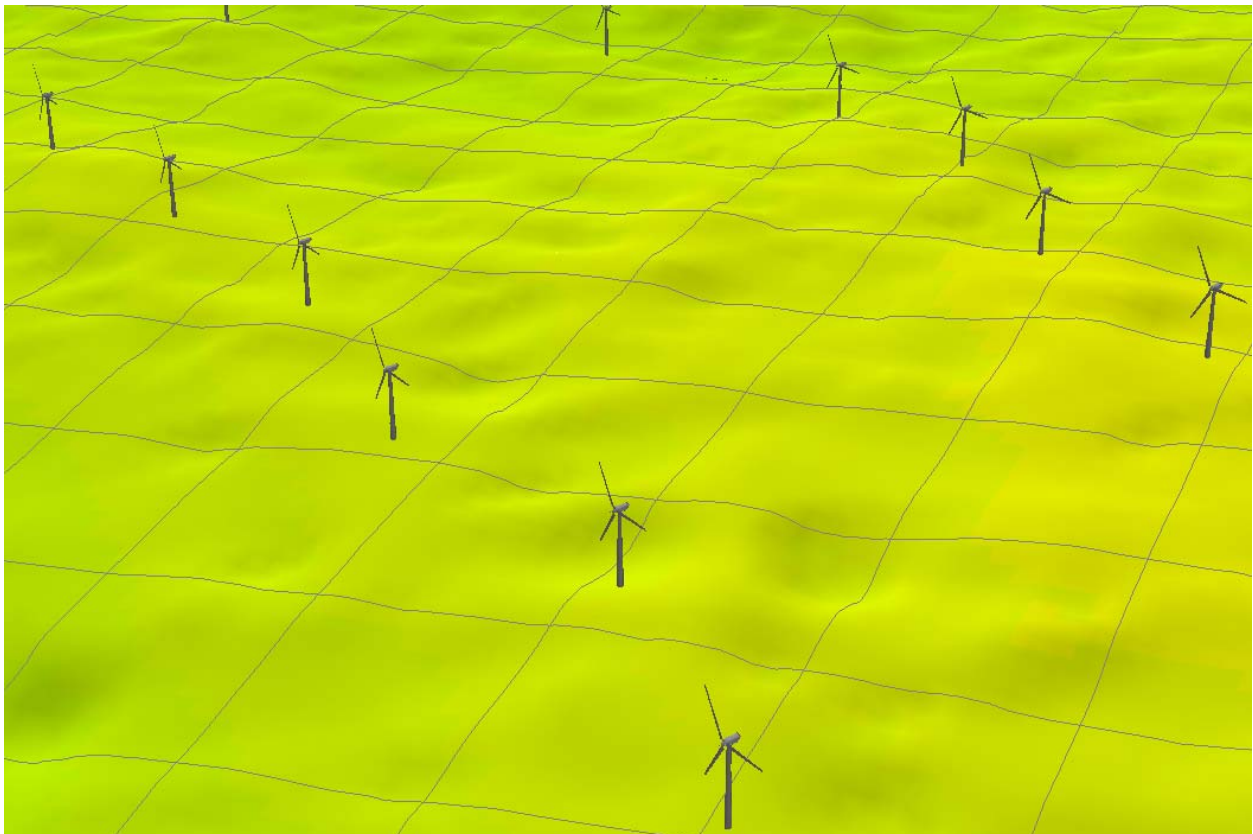
Pakline wind farm

Ljubusa wind farm

Client:

Kamen Dent d.o.o.

Mostar, BiH



June 2009

Document: **Preliminary layout report**
 Kupres wind farm
 Pakline wind farm
 Ljubusa wind farm

Client: Kamen Dent d.o.o.
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1. LOCATION DESCRIPTION

1.1. Location description and satellite images

Tomislavgrad – city and regional center situated in southern part of BiH on the crossroads connecting Mostar-Bihac-Banja Luka and Split-Sarajevo, with region spreading over 966 km², represents geographical and historical connection between Bosnia, Hercegovina and Dalmatia. Neighboring region of Kupres, with 600 km² became one of the smallest regions in BiH.

Situated on mountain area of Dinaridi, regions of Tomislavgrad and Kupres experience similar climate regimes, characterized by different, sometimes opposed influences of Mediterranean, continental and mountain climate. That mixture of influences result in warm summers and occasionally very harsh winters. This area is known to be highly windy with continental northern and maritime southern wind resulting in 65 – 70 % windy days during the year.

More potential zones are found meeting the energy demand for wind energy exploitation. In Kupres region the most interesting are hilltops of Borova kosa, Gradina and hill region southwest from the Ravanjsko field, continuing to Pakline and Ljubusa ridges in Tomislavgrad region. Complete area of planed wind farm is detritus with deficient vegetation, due to the cold winters and strong northern wind.

Location of wind farm Kupres is situated on the hilltops of Borova kosa (1368 m), Crljenac (1244 m), Kalpak (1195) and Podovi (1299 m) near the villages Gornji Musici and Gornje Ravno on the north, and hilltops Mala kozjaca (1197 m), Velika kozjaca (1220 m), Vucina (1162 m), Jastrebovac (1277 m) on the southwest from the Ravanjsko field. Access to location is by Tomislavgrad-Rama road that passes trough planed location. Whole area is available with cross country vehicle.

Location of wind farm Pakline continues further to the southwest, situating on the hilltops northeast from the Tomislavgrad. Significant are hilltops Ostra glava (1209 m), Javorina (1202 m), Dubokovac (1247 m), Ostra kosa (1294 m), Ciganluk (1331 m) and Derustica (1282 m) with villages Mokronoge, Lug, Kuk, Sarajlije and Letka in its foothill. Main access to location is by Tomislavgrad-Rama road on its northern part but there are more available paths from around villages passable with cross country vehicle.

Location of wind farm Ljubusa continues further on the south, cca 2 km northeast from villages Oplecani, Srdani, Rascani and Mandino selo, as a continuation of Pakline hill ridges. Significant are hilltops Magljen (1328 m), Ostra glavica (1318 m) and Velika kosa (1342 m). One of the access roads is gravel road from village Srdani passable with cross country vehicle.

Grid connection, considering the planed wind farm capacities has to be carried out on high voltage. Connection to 110 kV power line Tomislavgrad-Rama that passes trough northern part of planed wind farm Pakline and wind farm Kupres is recognized as one of the possible solutions for energy evacuation.



Figure 1-1 Photos of characteristic landscape



Figure 1-2 Satellite image with locations of wind farms

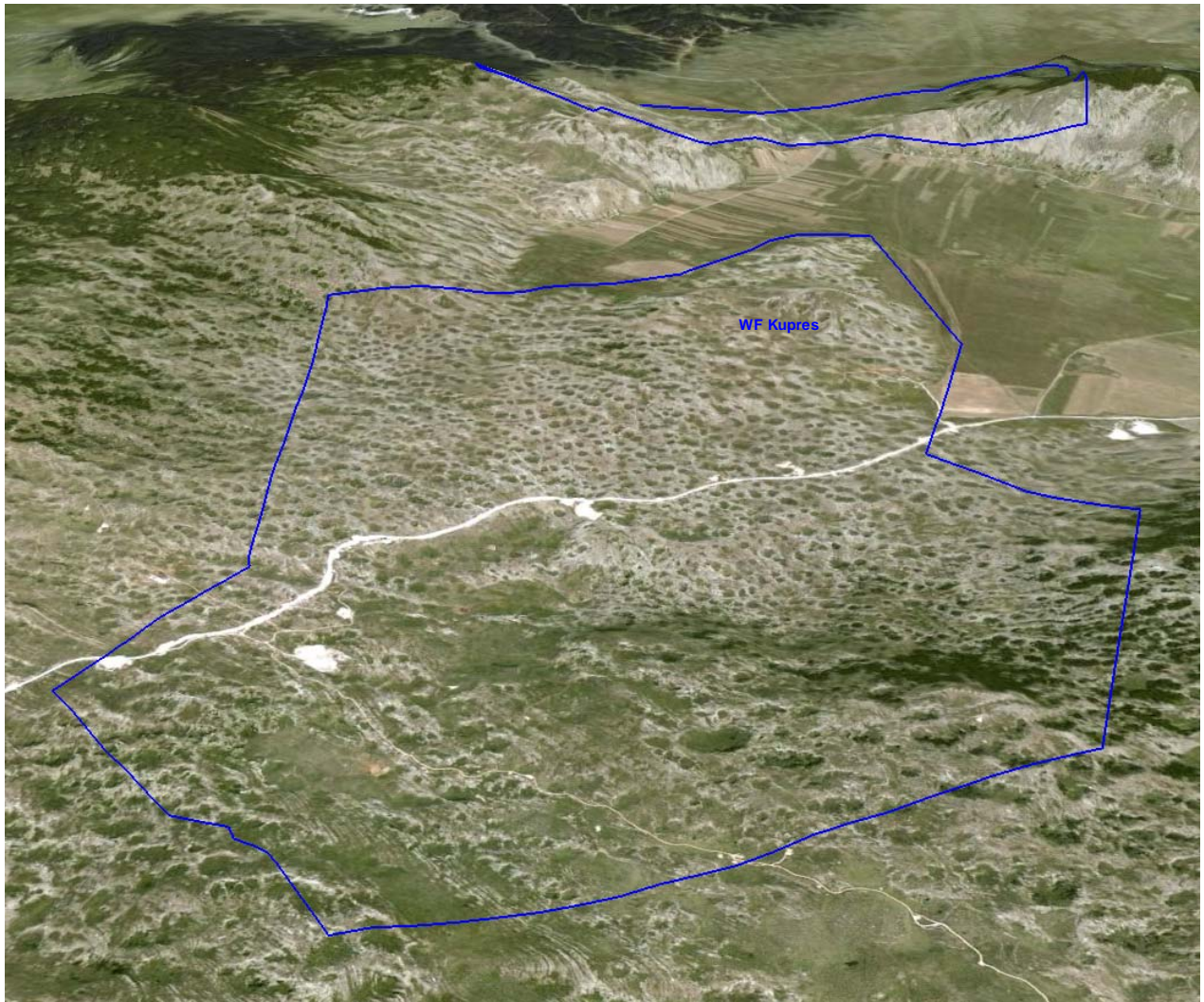


Figure 1-3 Satellite image of WF Kupres location

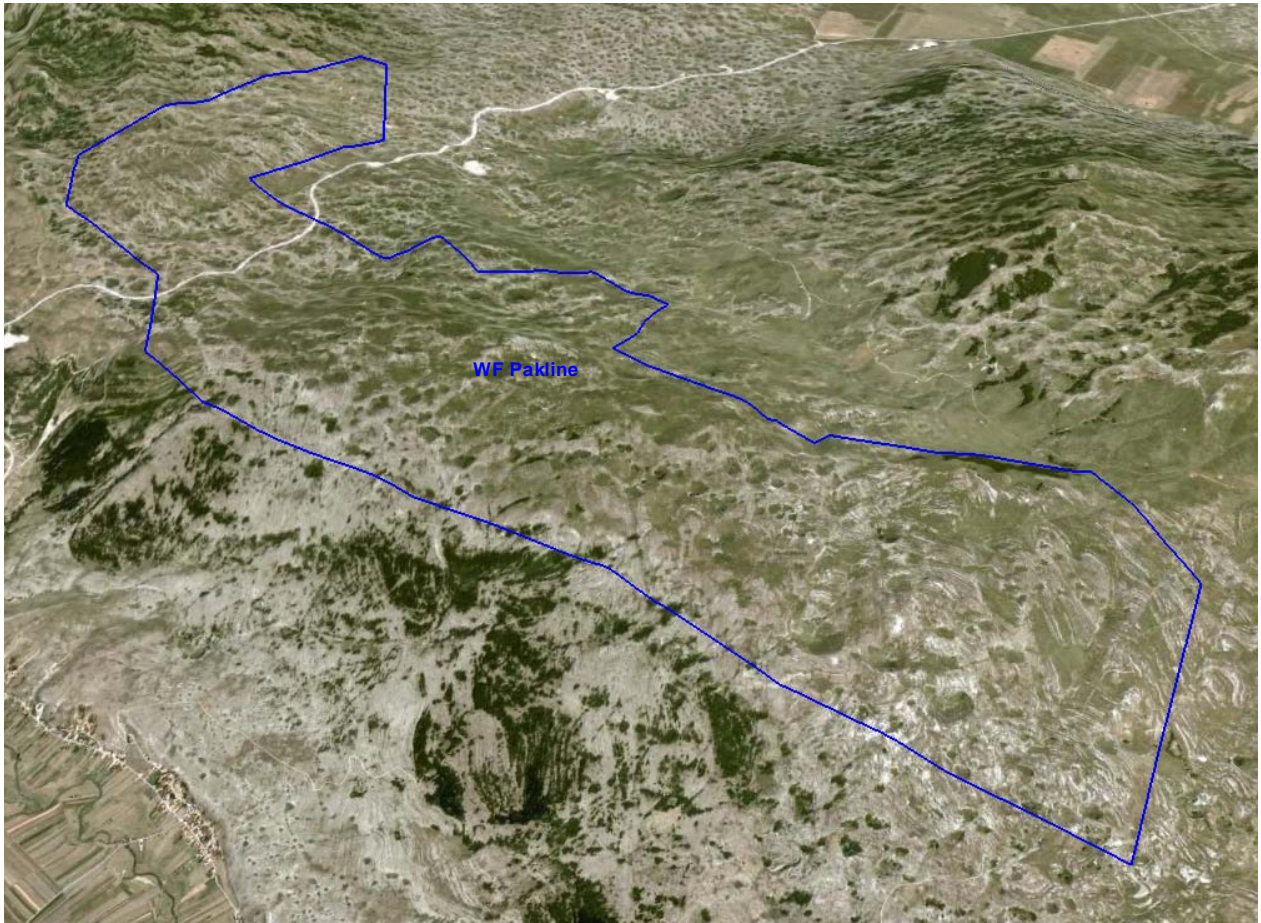


Figure 1-4 Satellite image of WF Pakline location



Figure 1-5 Satellite image of WF Ljubusa location

1.2. 3D terrain visualization in ArcGis software

Design of high quality 3D topography model of location is done with following:

- Control and correction of topography contours in 10 meter heights in order to create precise and smooth surface
- Forming a TIN (triangular regular network) using the vectorized contours as input
- Creating a raster surface over TIN allowing color graduation
- Importing significant objects such as geographic grids and infrastructure objects
- Creating terrain cross-sections

Considering the dominant wind direction of approximately 52° , as observed from the wind frequency distribution, cross-sections of planed wind farm areas are extracted from the height graduated map in 3km intervals.

Detailed visual insight in position and topographic characteristics of planed wind farm locations is given through satellite images, height graduated map and terrain cross-sections.

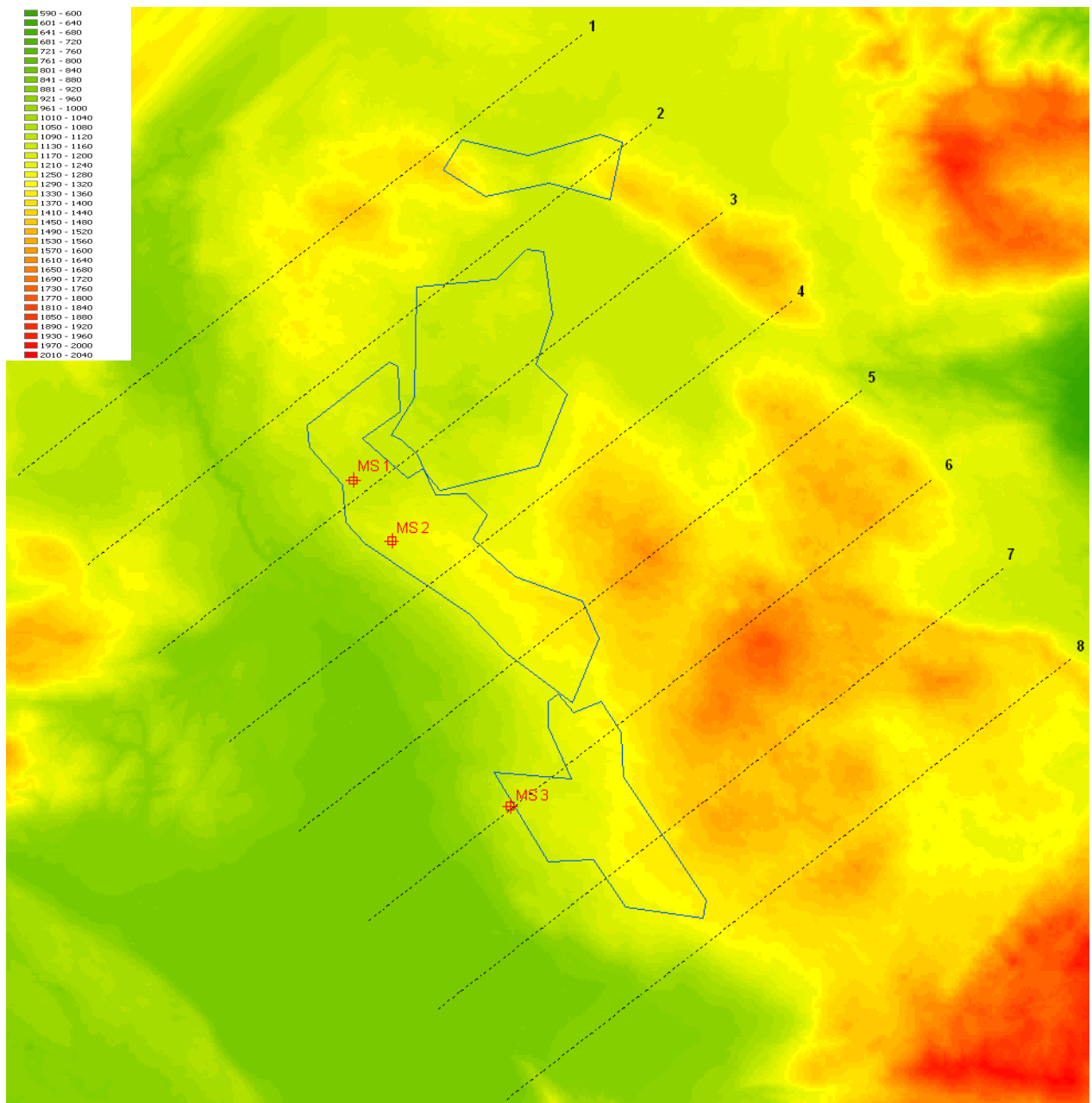


Figure 1-6 Height graduated map of wind farms location with cross-section tracks

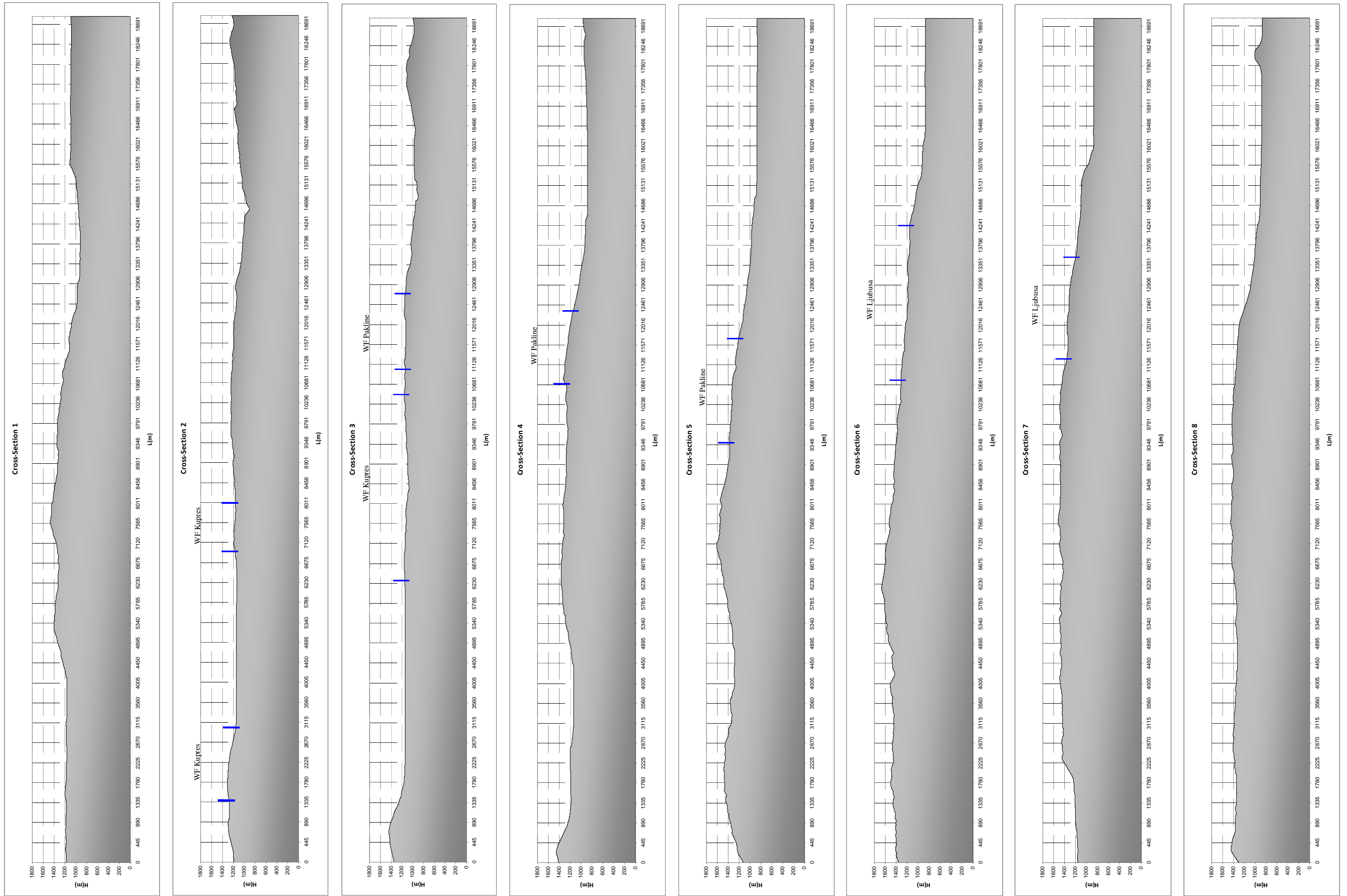


Figure 1-7 Terrain cross-sections

2. SITE MEASUREMENT DATA

For the following analysis, data from wind measurements over three sites are used. Data were delivered to Fractal by Kamen Dent. File format of data is “raw data” (NRG raw files, Wilog raw files) and scaled format.

The meteorological mast MS1 collapsed during the storm, October 2006. Masts MS2 and MS3 are still present at the site locations but are no longer operable.

There is substantial uncertainty in using the collected data, as the sites were not properly maintained and monitored. Also, installation reports for MS2 and MS3 are not available and some analysis parameters (wind vane offsets) are estimated by visual inspection of the masts.

2.1. Site measurement configurations and data quality

MS1

Site measurement configuration is extracted from a installation report (Installation report for locations Pakline and Ravanjska, Fractal d.o.o., Split, August 2007). Data from MS1 were received directly (email) from NRG logger on Fractal email account. The major data uncertainty source are installation effects of tower and surrounding terrain.

| General information | |
|-------------------------------|---|
| Measurement name | MS1 |
| Location name | Pakline |
| Location description | Pakline is located 8.2 km N-NE from Tomislavgrad town |
| Location position / height | E: 6440148 N: 6440148 ; 17.25128E 43.79119N /1161 |
| Location magnetic declination | 2.5° |
| Monitoring system | 50m tube tower (made by Kamen-dent) / NRG Data Logger |

| Measurement equipment | |
|------------------------------------|-------------------------------------|
| Anemometer 1 | NRG #40 – Calibration number #32673 |
| Measurement height/mounting | 50m / installed on boom |
| Anemometer 2 | NRG #40 – Calibration number #32674 |
| Measurement height/mounting | 25m / installed on boom |
| Wind Vane 1 | NRG #200P |
| Measurement height/mounting/offset | 48m / installed on boom / 45.5° |

| Data metrics | |
|------------------|---|
| Measuring period | 16.01.2007 - 18.10.2007 (276 days), without major data gaps |
| Averaging time | 10min |

There is a direction gap in data due relatively large wind vane dead band:

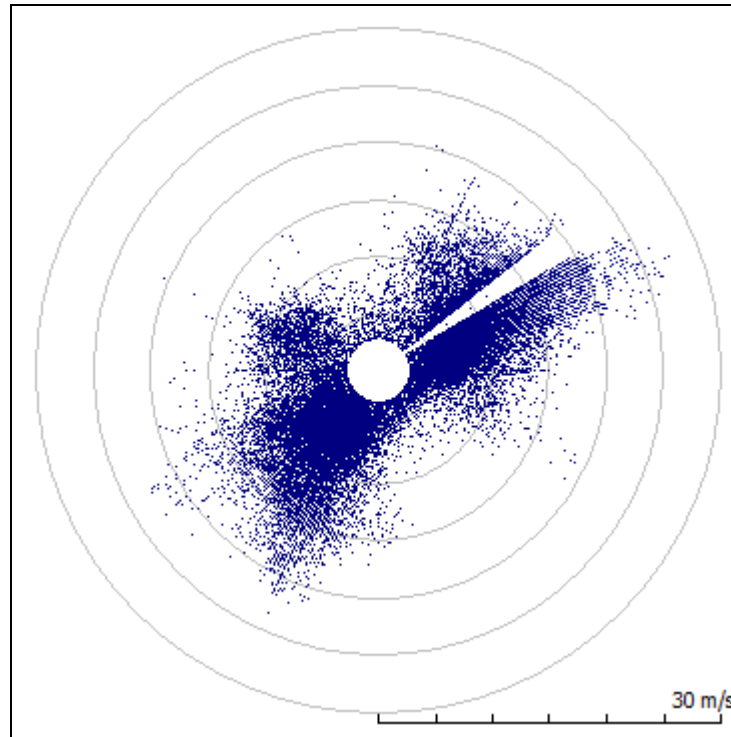


Figure 2-1 Observed wind speed vs. direction data for location MS1

MS2

There is no installation report available for MS2 site. The following site measurement configuration data is reconstructed by Fractal d.o.o. during the site inspection visit, 12.06.2009, and from Wilog raw data files delivered by Kamen Dent. Data collection for MS2 was not monitored by Fractal. Wind vane offsets are estimated by visual inspection of the mast.

Mast MS2 operated for a short period (162days). Because it is located in very close proximity of MS1, it is primarily used to validate the measurements from MS1, and to extend (MCP) analysis data for MS1.



Figure 2-2 MS2 mast

| General information | |
|--------------------------------------|---|
| Measurement name | MS2 |
| Location name | Mokronoge |
| Location description | Mokronoge is located 7.2 km N-NE from Tomislavgrad town |
| Location position GK ;WGS84 / height | E:6441170 N:4848323 ; 17.26416E 43.77697N /1226m |
| Location magnetic declination | 2.5° |
| Monitoring system | 50m tube tower / NRG Data Logger |

| Measurement equipment | |
|------------------------------------|--------------------------------|
| Anemometer 1 | Thies "First class" |
| Measurement height/mounting | 50m / top mounted |
| Anemometer 2 | Thies "First class" |
| Measurement height/mounting | 30m / installed on boom |
| Wind Vane 1 | Thies "Compact" |
| Measurement height/mounting/offset | 50m / top mounted / -72° |
| Wind Vane 2 | Thies "Compact" |
| Measurement height/mounting/offset | 30m / installed on boom / -35° |

| Data metrics | |
|---------------------|---|
| Measuring period | 23.12.2006-3.06.2007 (162 days), without major data gaps |
| Averaging time | 10min |
| Other records | Temperature |

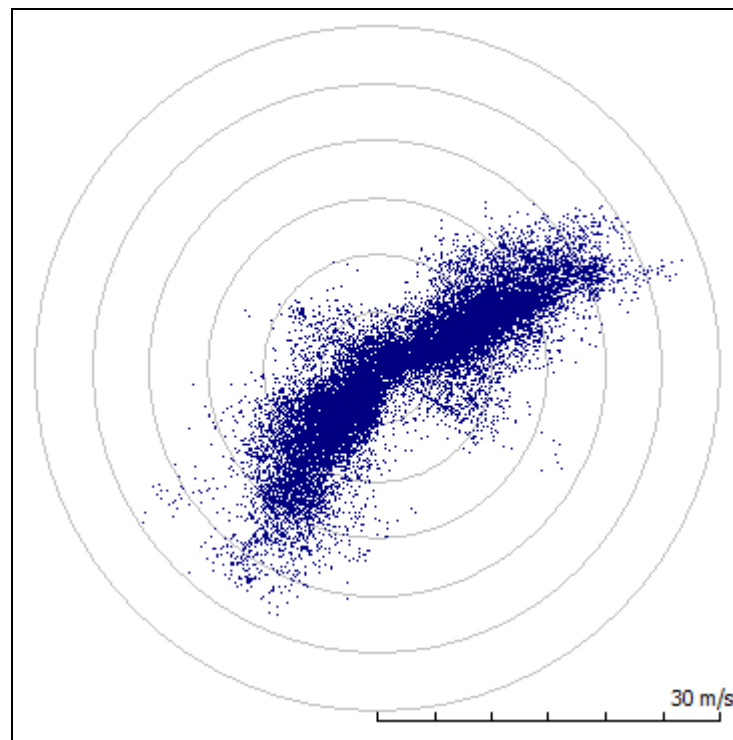


Figure 2-3 Observed wind speed vs. direction data for location MS2

MS3

There is no installation report available for MS3 site. The following site measurement configuration data is reconstructed by Fractal during the site inspection visit, 12.06.2009, and from raw data files delivered by Kamen Dent. Data collection for MS3 was not monitored by Fractal. Wind vane offsets are estimated by visual inspection of the mast.



Figure 2-4 MS3 mast

| General information | |
|--------------------------------------|--|
| Measurement name | MS3 |
| Location name | Srdane |
| Location description | Srdane is located 6.3 km E from Tomislavgrad town |
| Location position GK ;WGS84 / height | E: 6444313 N:4841294 ; 17.30393E 43.71395N / 1163m |
| Location magnetic declination | 2.5° |
| Monitoring system | 50m tube tower / Wilmers messtechnik - Wilog 306 |

| Measurement equipment | |
|------------------------------|------------------------------|
| Anemometer 1 | Thies "First class" |
| Measurement height/mounting | 50m / top mounted |
| Anemometer 2 | Thies "First class" |
| Measurement height/mounting | 30m / installed on boom |
| Anemometer 3 | Thies "First class" |
| Measurement height/mounting | 30m / installed on boom |
| Wind Vane 1 | Thies "Compact" / -4.3° |
| Measurement height/mounting | 50m / top mounted |
| Wind Vane 2 | Thies "Compact" |
| Measurement height/mounting | 30m / installed on boom / 5° |
| Wind Vane 3 | Thies "Compact" |
| Measurement height/mounting | 30m / installed on boom / 5° |

| Data metrics | |
|---------------------|---|
| Measuring period | 11.10.2006-1.07.2008 (453 days), without major data gaps |
| Averaging time | 10min |
| Other records | Temperature |

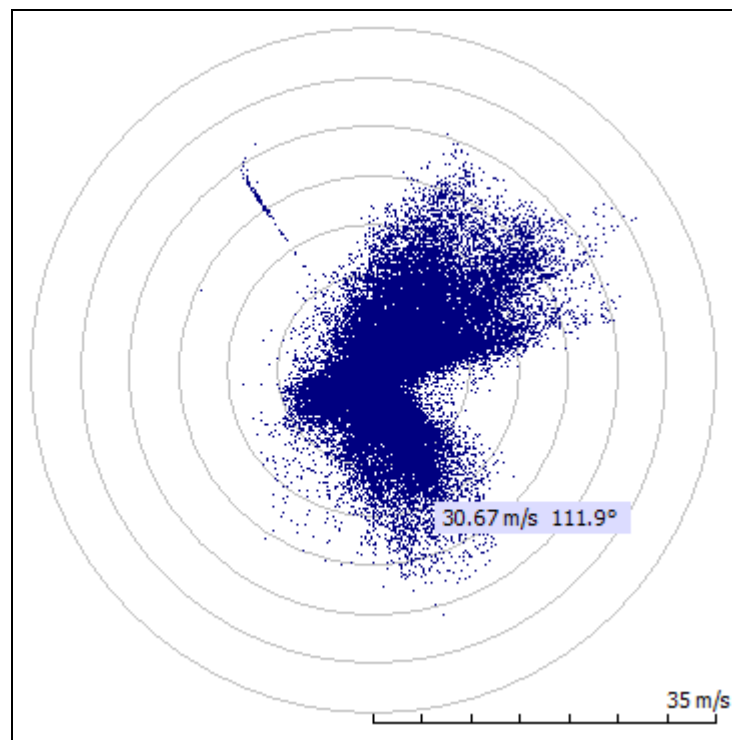


Figure 2-5 Observed wind speed vs. direction data for location MS3

2.2. Wind measurement analysis and report: MS1 (h=50m)

The measurement period for meteorological mast at location MS1 was from 16.01.2007 to 18.10.2007 (276 days).

MCP method (least squares method) is used to derive one year representative wind speed and direction frequency. The first source for MCP were data from the nearby meteorological mast MS2. Using MS2, analysis data are extended only for 24 days (during the windy period and with a very high correlation). For remaining missing periods, MCP derived data from meteorological mast MS3 are used. Turbulence analysis is performed only with original MS1-Pakline data.

Table 2-1 MCP reconstruction of analysis data

| Period | Analysis data source | Duration |
|------------------------------|----------------------|--------------------|
| 01.11.2006-31.10.2007 | | 1 year = 8760hours |
| 01.11.2006-22.11.2006 | MCP from MS3 | 52 days |
| 23.12.2006-15.01.2007 | MCP from MS2 | 24 days |
| 16.01.2007-18.10.2007 | Original MS1 | 276 days |
| 19.10.2007-31.10.2007 | MCP from MS3 | 13 days |

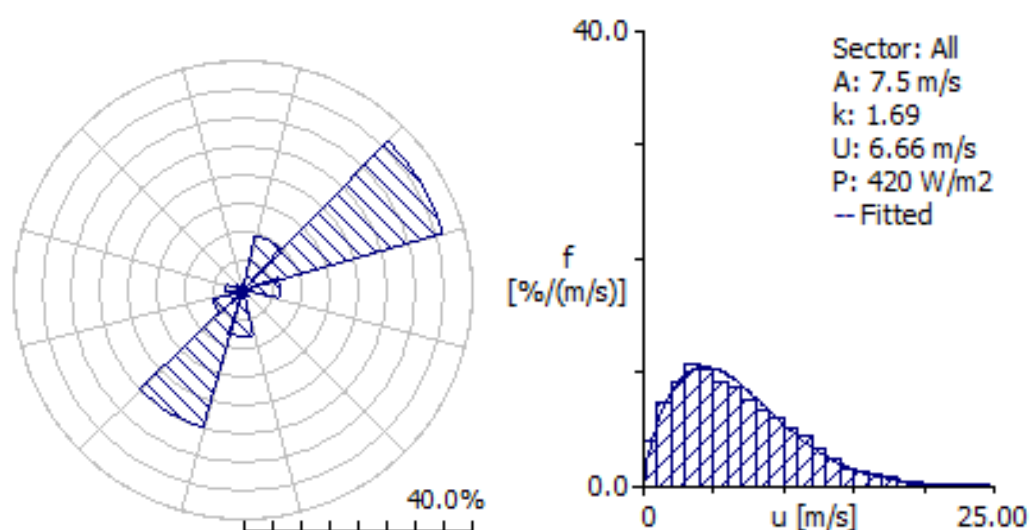


Figure 2-6 Wind Rose (Left) and Weibull Distribution for all directions (Right) for MS1

Table 2-2 MS1 - Observed wind climate - 01.11.2006-31.10.2007

| Sector | | Wind climate | | | | Power |
|----------------|-----------|---------------|-----------------|-----------|------------------|-----------------------------------|
| number | angle [°] | frequency [%] | Weibull-A [m/s] | Weibull-k | mean speed [m/s] | power density [W/m ²] |
| 1 | 0 | 1.0 | 5.6 | 1.53 | 5.06 | 210 |
| 2 | 30 | 9.7 | 9.2 | 2.29 | 8.17 | 565 |
| 3 | 60 | 36.1 | 9.5 | 2.09 | 8.42 | 669 |
| 4 | 90 | 6.6 | 4.4 | 1.61 | 3.93 | 91 |
| 5 | 120 | 0.9 | 2.5 | 0.94 | 2.60 | 77 |
| 6 | 150 | 1.5 | 2.0 | 1.00 | 2.04 | 31 |
| 7 | 180 | 8.2 | 5.4 | 1.30 | 4.98 | 259 |
| 8 | 210 | 25.0 | 6.6 | 1.66 | 5.89 | 295 |
| 9 | 240 | 5.8 | 6.1 | 1.64 | 5.45 | 237 |
| 10 | 270 | 3.2 | 5.4 | 2.08 | 4.80 | 125 |
| 11 | 300 | 1.6 | 5.2 | 2.43 | 4.58 | 95 |
| 12 | 330 | 0.5 | 2.6 | 1.23 | 2.42 | 33 |
| All (emergent) | | | | | 6.63 | 420 |

As depicted, at the MS1 site the wind direction distribution is strongly bipolar in that the wind is from the NE or the SW nearly all of the time.

Average/min/max annual temperature: -8.9/10.2/34.7 °C

Table 2-3 Wind Speed and Direction Frequency Distribution at 50m (U[m/s])

| U | 0° | 30° | 60° | 90° | 120° | 150° | 180° | 210° | 240° | 270° | 300° | 330° | All |
|------|-----|-----|-----|-----|------|------|------|------|------|------|------|------|-----|
| 1.0 | 116 | 30 | 20 | 49 | 222 | 275 | 51 | 27 | 52 | 61 | 65 | 193 | 38 |
| 2.0 | 143 | 61 | 26 | 101 | 323 | 351 | 125 | 74 | 109 | 117 | 96 | 314 | 73 |
| 3.0 | 143 | 66 | 39 | 166 | 151 | 182 | 141 | 113 | 134 | 122 | 141 | 222 | 92 |
| 4.0 | 91 | 53 | 65 | 258 | 69 | 87 | 155 | 131 | 122 | 135 | 116 | 107 | 108 |
| 5.0 | 73 | 58 | 78 | 195 | 45 | 35 | 125 | 125 | 103 | 126 | 185 | 64 | 103 |
| 6.0 | 53 | 76 | 88 | 74 | 52 | 23 | 84 | 106 | 102 | 138 | 161 | 43 | 92 |
| 7.0 | 60 | 82 | 96 | 43 | 46 | 13 | 68 | 87 | 102 | 107 | 122 | 27 | 86 |
| 8.0 | 66 | 86 | 92 | 38 | 29 | 6 | 47 | 75 | 79 | 89 | 60 | 14 | 76 |
| 9.0 | 87 | 96 | 84 | 32 | 27 | 7 | 39 | 59 | 63 | 60 | 27 | 4 | 67 |
| 10.0 | 91 | 98 | 76 | 14 | 15 | 8 | 32 | 55 | 43 | 25 | 18 | 0 | 59 |
| 11.0 | 30 | 78 | 68 | 15 | 8 | 9 | 30 | 50 | 23 | 10 | 5 | 4 | 51 |
| 12.0 | 17 | 64 | 65 | 7 | 4 | 4 | 31 | 38 | 24 | 4 | 4 | 8 | 44 |
| 13.0 | 9 | 46 | 55 | 4 | 0 | 1 | 27 | 22 | 12 | 1 | 1 | 0 | 33 |
| 14.0 | 9 | 31 | 42 | 1 | 0 | 0 | 16 | 13 | 10 | 1 | 0 | 0 | 24 |
| 15.0 | 4 | 24 | 28 | 1 | 2 | 0 | 10 | 7 | 8 | 1 | 0 | 0 | 16 |
| 16.0 | 3 | 16 | 22 | 0 | 0 | 0 | 9 | 7 | 4 | 1 | 0 | 0 | 12 |
| 17.0 | 1 | 11 | 22 | 0 | 7 | 0 | 3 | 6 | 2 | 0 | 0 | 0 | 11 |
| 18.0 | 4 | 8 | 15 | 0 | 0 | 0 | 3 | 3 | 3 | 0 | 0 | 0 | 8 |
| 19.0 | 0 | 7 | 8 | 0 | 0 | 0 | 3 | 2 | 4 | 0 | 0 | 0 | 4 |
| 20.0 | 0 | 3 | 4 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| 21.0 | 0 | 4 | 3 | 0 | 0 | 0 | 0 | 1 | 1 | 0 | 0 | 0 | 2 |
| 22.0 | 0 | 1 | 2 | 0 | 0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 1 |
| 23.0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |
| 24.0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: The frequencies of occurrence in per mille

Turbulence intensity analysis

IEC61400-1 edition 2 defines the characteristic turbulence intensity I_{15} as the mean plus standard deviation of random ten-min measurements. Calculated values are shown in next table.

Table 2-4 Turbulence intensity analysis MS1 (h=50m) 16.01.2007-18.10.2007 (<1 year)

| Wind Speed [m/s] | Hours | Mean Turbulence Intensity | Standard Deviation of Turbulence Intensity | Characteristic Turbulence Intensity - I_{15} |
|------------------|-------|---------------------------|--|--|
| 4 | 766 | 0.126 | 0.076 | 0.202 |
| 5 | 727 | 0.116 | 0.064 | 0.179 |
| 6 | 670 | 0.107 | 0.053 | 0.160 |
| 7 | 629 | 0.096 | 0.048 | 0.144 |
| 8 | 551 | 0.092 | 0.046 | 0.138 |
| 9 | 471 | 0.093 | 0.041 | 0.133 |
| 10 | 402 | 0.096 | 0.038 | 0.134 |
| 11 | 334 | 0.095 | 0.033 | 0.128 |
| 12 | 277 | 0.094 | 0.031 | 0.126 |
| 13 | 185 | 0.089 | 0.031 | 0.120 |
| 14 | 107 | 0.093 | 0.034 | 0.127 |
| 15 | 70 | 0.095 | 0.030 | 0.125 |
| 16 | 50 | 0.098 | 0.026 | 0.124 |
| 17 | 38 | 0.092 | 0.027 | 0.119 |
| 18 | 22 | 0.088 | 0.027 | 0.115 |
| 19 | 8 | 0.097 | 0.035 | 0.132 |
| 20 | 4 | 0.085 | 0.030 | 0.115 |
| 21 | 5 | 0.068 | 0.023 | 0.092 |
| 22 | 4 | 0.062 | 0.015 | 0.077 |
| 23 | 1 | 0.064 | 0.016 | 0.079 |
| 24 | 1 | 0.065 | 0.009 | 0.075 |
| 25 | 0 | 0.061 | 0.001 | 0.061 |

2.3. Wind measurement analysis and report: MS3 (h=50m)

The measurement period for meteorological mast at location MS3 was 11.10.2006-1.07.2008 (453 days). To be comparable with data from MS1, one year from 01.11.2006-31.10.2007 is used for analysis.

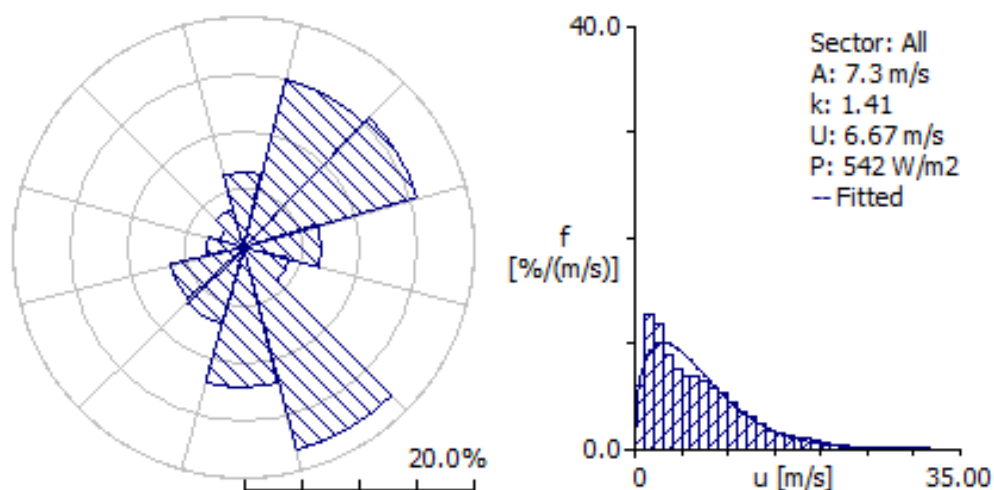


Figure 2-7 Wind Rose (Left) and Weibull Distribution for all directions (Right) for MS3

Table 2-5 MS3 - Observed wind climate - 01.11.2006-31.10.2007

| Sector | | Wind climate | | | | Power |
|----------------|-----------|---------------|-----------------|-----------|------------------|-----------------------------------|
| number | angle [°] | frequency [%] | Weibull-A [m/s] | Weibull-k | Mean speed [m/s] | power density [W/m ²] |
| 1 | 0 | 6.6 | 6.9 | 1.63 | 6.19 | 351 |
| 2 | 30 | 15.0 | 9.8 | 1.88 | 8.73 | 832 |
| 3 | 60 | 15.5 | 11.0 | 1.81 | 9.74 | 1202 |
| 4 | 90 | 6.7 | 7.4 | 1.60 | 6.62 | 441 |
| 5 | 120 | 4.0 | 3.4 | 1.01 | 3.38 | 138 |
| 6 | 150 | 18.2 | 8.0 | 1.73 | 7.17 | 507 |
| 7 | 180 | 12.0 | 6.5 | 1.36 | 5.93 | 406 |
| 8 | 210 | 6.8 | 4.2 | 1.31 | 3.84 | 117 |
| 9 | 240 | 6.4 | 5.3 | 2.09 | 4.66 | 113 |
| 10 | 270 | 3.2 | 3.4 | 1.39 | 3.11 | 56 |
| 11 | 300 | 2.2 | 2.6 | 1.23 | 2.43 | 34 |
| 12 | 330 | 3.3 | 3.7 | 0.85 | 4.07 | 387 |
| All (emergent) | | | | | 6.68 | 542 |

As depicted, at the MS3 site the wind direction distribution is bipolar in that the wind is from the NE or the S-SSE most of the time.

Average/min/max annual temperature is not calculated as no 1-year data are available.

Table 2-6 Wind Speed and Direction Frequency Distribution at 50m (U[m/s])

| U | 0° | 30° | 60° | 90° | 120° | 150° | 180° | 210° | 240° | 270° | 300° | 330° | All |
|------|-----|-----|-----|-----|------|------|------|------|------|------|------|------|-----|
| 1.0 | 44 | 36 | 60 | 129 | 159 | 27 | 31 | 57 | 49 | 115 | 147 | 120 | 59 |
| 2.0 | 121 | 86 | 74 | 112 | 274 | 92 | 114 | 164 | 138 | 274 | 359 | 249 | 126 |
| 3.0 | 120 | 72 | 42 | 76 | 170 | 117 | 160 | 228 | 147 | 184 | 213 | 166 | 119 |
| 4.0 | 114 | 58 | 40 | 63 | 88 | 86 | 115 | 164 | 117 | 131 | 105 | 114 | 89 |
| 5.0 | 76 | 46 | 47 | 77 | 65 | 75 | 100 | 115 | 128 | 82 | 79 | 89 | 76 |
| 6.0 | 75 | 54 | 48 | 60 | 49 | 66 | 74 | 87 | 136 | 75 | 46 | 70 | 68 |
| 7.0 | 75 | 66 | 64 | 80 | 40 | 82 | 60 | 58 | 113 | 54 | 19 | 52 | 69 |
| 8.0 | 74 | 75 | 67 | 65 | 30 | 78 | 56 | 39 | 85 | 49 | 11 | 31 | 64 |
| 9.0 | 66 | 81 | 66 | 58 | 32 | 66 | 47 | 30 | 52 | 24 | 12 | 21 | 56 |
| 10.0 | 64 | 77 | 60 | 73 | 26 | 68 | 45 | 22 | 21 | 9 | 4 | 16 | 53 |
| 11.0 | 43 | 67 | 62 | 52 | 21 | 54 | 45 | 10 | 8 | 2 | 1 | 11 | 44 |
| 12.0 | 34 | 51 | 47 | 45 | 12 | 48 | 39 | 4 | 2 | 1 | 2 | 5 | 35 |
| 13.0 | 30 | 48 | 50 | 31 | 14 | 41 | 31 | 7 | 2 | 0 | 0 | 1 | 31 |
| 14.0 | 19 | 36 | 41 | 25 | 7 | 26 | 21 | 4 | 2 | 1 | 0 | 0 | 23 |
| 15.0 | 17 | 26 | 37 | 17 | 5 | 18 | 16 | 3 | 1 | 0 | 0 | 1 | 18 |
| 16.0 | 11 | 23 | 31 | 13 | 6 | 14 | 10 | 2 | 0 | 0 | 0 | 0 | 14 |
| 17.0 | 8 | 21 | 33 | 7 | 2 | 13 | 10 | 2 | 0 | 0 | 0 | 3 | 13 |
| 18.0 | 5 | 21 | 27 | 4 | 0 | 10 | 10 | 2 | 0 | 0 | 0 | 2 | 11 |
| 19.0 | 2 | 19 | 27 | 2 | 0 | 6 | 6 | 1 | 0 | 0 | 0 | 3 | 9 |
| 20.0 | 1 | 13 | 23 | 2 | 0 | 4 | 4 | 1 | 0 | 0 | 1 | 8 | 7 |
| 21.0 | 1 | 12 | 19 | 1 | 0 | 3 | 3 | 0 | 0 | 0 | 0 | 8 | 6 |
| 22.0 | 1 | 6 | 13 | 3 | 0 | 3 | 2 | 0 | 0 | 0 | 0 | 11 | 4 |
| 23.0 | 0 | 4 | 9 | 2 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 10 | 3 |
| 24.0 | 0 | 3 | 5 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 5 | 1 |
| 25.0 | 0 | 1 | 4 | 2 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 2 | 1 |
| 26.0 | 0 | 0 | 2 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 27.0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 1 | 0 |
| 28.0 | 0 | 0 | 1 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 | 0 |

Note: The frequencies of occurrence in per mille.

Turbulence intensity analysis

IEC61400-1 edition 2 defines the characteristic turbulence intensity I_{15} as the mean plus standard deviation of random ten-min measurements. Calculated values are shown in next table.

Table 2-7 Turbulence intensity analysis MS3 (h=50m) 01.11.2006-31.10.2007

| Wind Speed [m/s] | Hours | Mean Turbulence Intensity | Standard Deviation of Turbulence Intensity | Characteristic Turbulence Intensity - I_{15} |
|------------------|-------|---------------------------|--|--|
| 4 | 703 | 0.171 | 0.103 | 0.274 |
| 5 | 609 | 0.154 | 0.090 | 0.244 |
| 6 | 592 | 0.137 | 0.081 | 0.218 |
| 7 | 608 | 0.125 | 0.067 | 0.192 |
| 8 | 522 | 0.119 | 0.061 | 0.180 |
| 9 | 467 | 0.115 | 0.057 | 0.172 |
| 10 | 418 | 0.111 | 0.053 | 0.164 |
| 11 | 350 | 0.108 | 0.046 | 0.154 |
| 12 | 279 | 0.108 | 0.047 | 0.155 |
| 13 | 244 | 0.106 | 0.049 | 0.155 |
| 14 | 177 | 0.107 | 0.049 | 0.157 |
| 15 | 133 | 0.107 | 0.044 | 0.152 |
| 16 | 116 | 0.108 | 0.044 | 0.152 |
| 17 | 107 | 0.106 | 0.037 | 0.143 |
| 18 | 93 | 0.101 | 0.033 | 0.134 |
| 19 | 70 | 0.095 | 0.029 | 0.124 |
| 20 | 60 | 0.091 | 0.027 | 0.118 |
| 21 | 46 | 0.084 | 0.026 | 0.110 |
| 22 | 29 | 0.084 | 0.026 | 0.110 |
| 23 | 18 | 0.075 | 0.026 | 0.101 |
| 24 | 9 | 0.070 | 0.021 | 0.091 |
| 25 | 6 | 0.067 | 0.024 | 0.090 |

The MS3 site has much higher turbulence intensity values than MS1. The increased turbulence level might be due the MS3 placement at the edge of the hill.

3. LAYOUT CALCULATION METHODOLOGY

Analyses is made in two steps, using:

- WASP software to determine site wind climate conditions from topography and measurement data from reference sites. The map of wind resource over the area is generated in the form of standard WRG file (wind resource grid) containing Weibull distribution parameters for each of direction sectors.
- WindFarmer software for layout optimization, using topography model, observed wind data and wind resource grid data from WASP.

Layout calculation and optimization is also a influenced by all uncertainties introduced with input data.

3.1. WASP site wind climate

In order to calculate WRG , the WASP model considered:

For all sites:

- WASP 9.01 default project parameters.
- Uniform roughness length of 0.03 m.
- Topography: a terrain map with 10m level contours.
- 25m resolution and 80m hub height.

For particular sites:

- Wind farm Kupres measurement data:
A full year (8,760 hours) of data from MS1(276days) + MCP from MS2(24 days) and MS3(52days).
- Wind farm Pakline measurement data:
A full year (8,760 hours) of data from MS1 (276days) +MCP from MS2(24 days) and MS3(52days).
- Wind farm Ljubusa measurement data:
A full year (8,760 hours) of data from MS3.

3.2. Layout optimization using WindFarmer software

- Part of data used in energy calculation is loaded from WASP in the form of WRG file. Frequency table is associated to correct the error generated by the use of weibull approximation of wind speed and direction distribution in WRG file.
- Other data used in energy calculation purposes, as annual mean temperature, site reference air density and site roughness index, has been derived from collected data or observed during the location visit.

- Data used in turbulence intensity calculations has also been derived from collected data in the form of mean value of turbulence intensity and standard deviation of wind speed standard deviation. Considering that mast MS1, used as a reference site for WF Kupres and WF Pakline, has not completed the whole-year measurement, turbulence has been calculated just as a function of wind speed. For measurement mast MS2 used as reference site for WF Ljubusa, turbulence experienced at mast position has been calculated as a function of both wind speed and direction.
- Restrictions defined for layout optimization consider dwellings, roads and power lines exclusion zones as defined in regulations regarding wind power generator placement.
- Optimization is made by WF taking into account speed-up topography effects and wake effect by Modified Park and Eddy Viscosity Model. Due to its simplicity and faster calculation, Modified Park model has been used during the process of optimization. Advanced Eddy Viscosity model has been used for final energy calculation.
- Also, optimization is partly made manually, changing the number of wind turbines to determine their optimal number due to specific energy yield.
- Turbulence intensity according to IEC 61400-1 Ed2 standard at each turbine position is also considered during the process of optimization in order to stay within wind turbine manufacturer design limits.
- Considering the prevailing wind directions, wake effects and observed turbulence intensity, turbine exclusion zones of min 4D/10D are used.

Complete analyses is made in three separate areas (WF Kupres, WF Pakline and WF Ljubusa), considering mutual wake effect.

Nominal power curve for Siemens SWT-2.3-93 was used for energy calculation, scaled on **selected height of 80m** and appropriate air density.

Cadastral maps are used in WF Pakline and WF Ljubusa areas for final manual wind turbine repositioning, in order to force state-owned land with negligible effect on energy yield.

3.3. Layout report content

Layout of Kupres, Pakline and Ljubusa WF is calculated separately and presented in chapters 4-6. Following data is provided:

- Map from AutoCAD showing the positions of measurement mast and wind farm area on topographic map 1:25000.
- Map from ArcGIS showing the positions of measurement mast and wind farm area on height graduated map.

- Two maps from WASP showing the wind speed and energy distribution from all sectors over the wind farm area.
- Table consisting the gross and net energy, wake losses, capacity factor and net energy index per unit for each wind turbine.
- Table consisting the number of wind turbines, total net energy, average energy per wind turbine, capacity factor and wake losses.
- Map from WindFarmer showing the wind turbine positions and 4D-10D elliptical separation distances on topographic map 1:25000 with transparent color graduated wind energy distribution and net energy indexes for each wind turbine.
- Turbulence table with estimated design turbulence intensity calculated according to IEC 61400-1 Ed2 standard, showing characteristic turbulence intensity experienced at hub height for each wind turbine.
- Map from WindFarmer showing the wind turbine positions and 4D-10D elliptical separation distances on topographic map 1:25000 with transparent color graduated wind energy distribution and estimated design turbulence intensity calculated according to IEC 61400-1 Ed2 standard for each wind turbine.
- Three-dimensional images from ArcGis showing the wind farm from direction of north, south, east and west.

In Appendix, the following maps are provided for each WF:

- Map from AutoCAD showing wind turbines and measurement mast positions on topographic map along with the table of wind turbine coordinates in Gauss-Kruger projection and altitudes.
- Map from AutoCAD showing wind turbines on cadastre map along with the table consisting cadastre numbers of particles that wind turbines are placed on.

3.4. File list

- This report
- Contours.dwg – AutoCAD file showing vectorized height contours
- MS Excel filtered data used in calculations
- MS Excel table of wind turbine coordinates
- WF_Kupres_Pakline_Ljubusa.dwg – AutoCAD file containing all graphical data used for layout

4. WIND FARM KUPRES LAYOUT

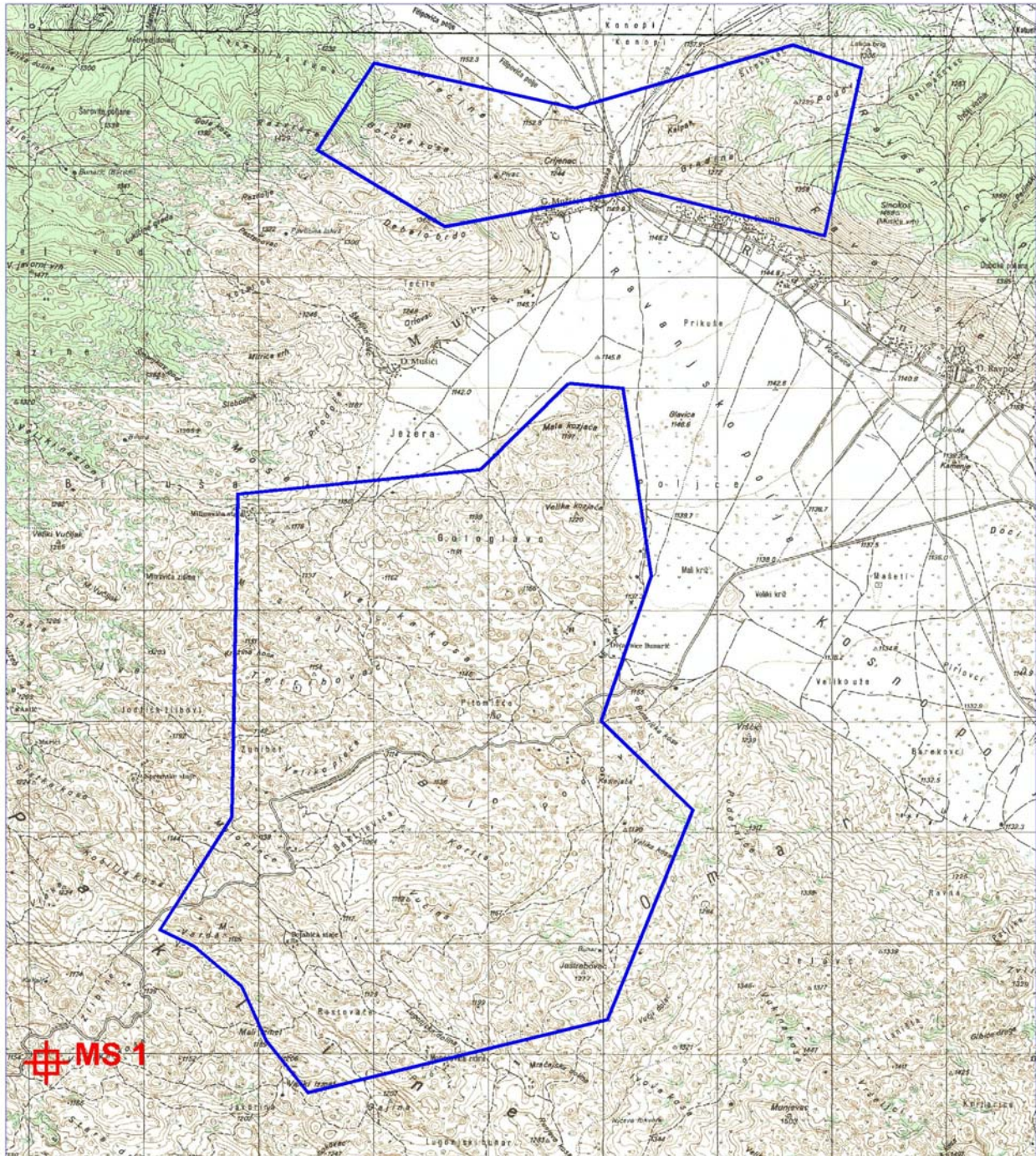


Figure 4-1 Topography map with planed wind farm area and mast position

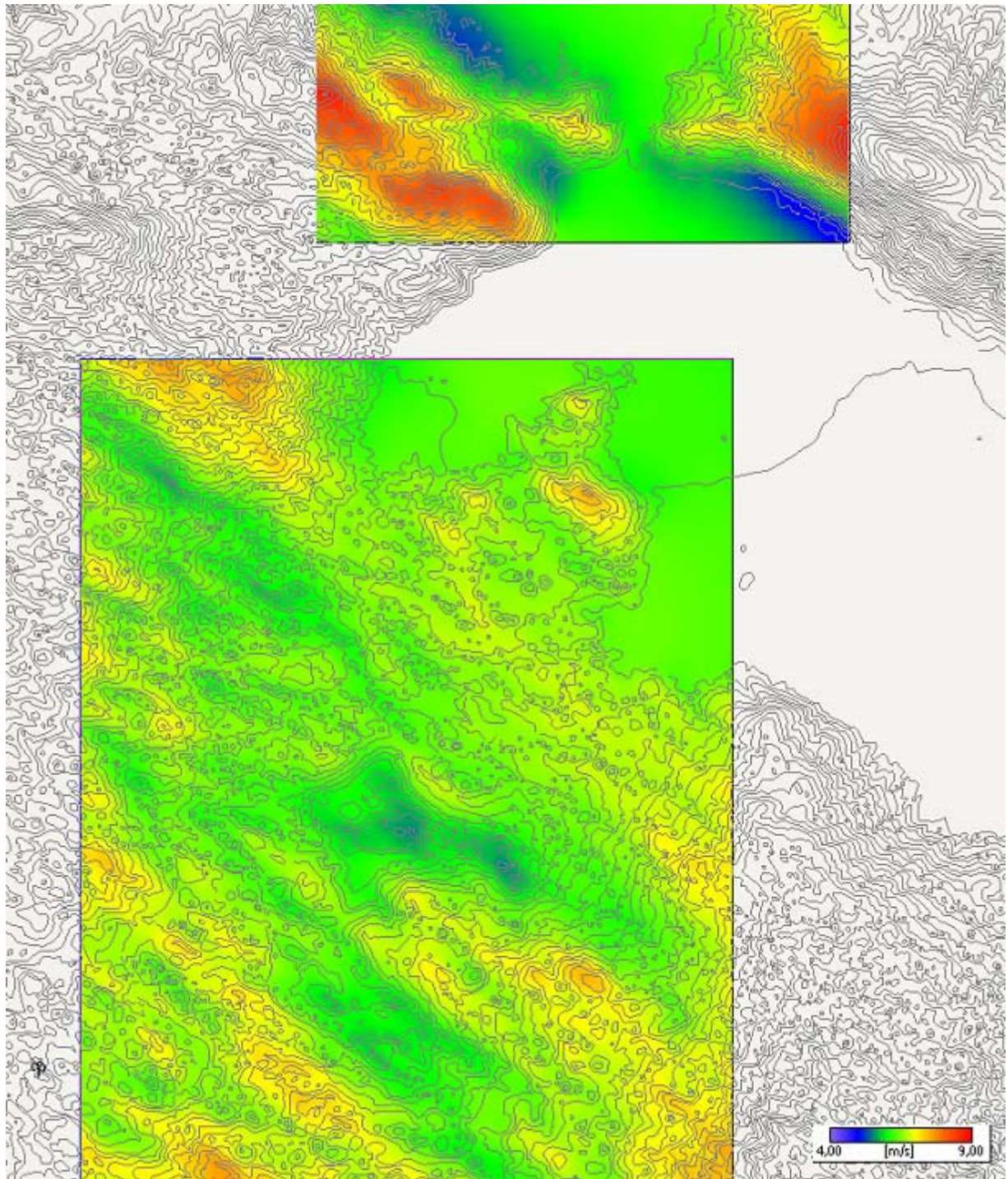


Figure 4-2 Wind speed distribution over the planned wind farm area (WAsP)

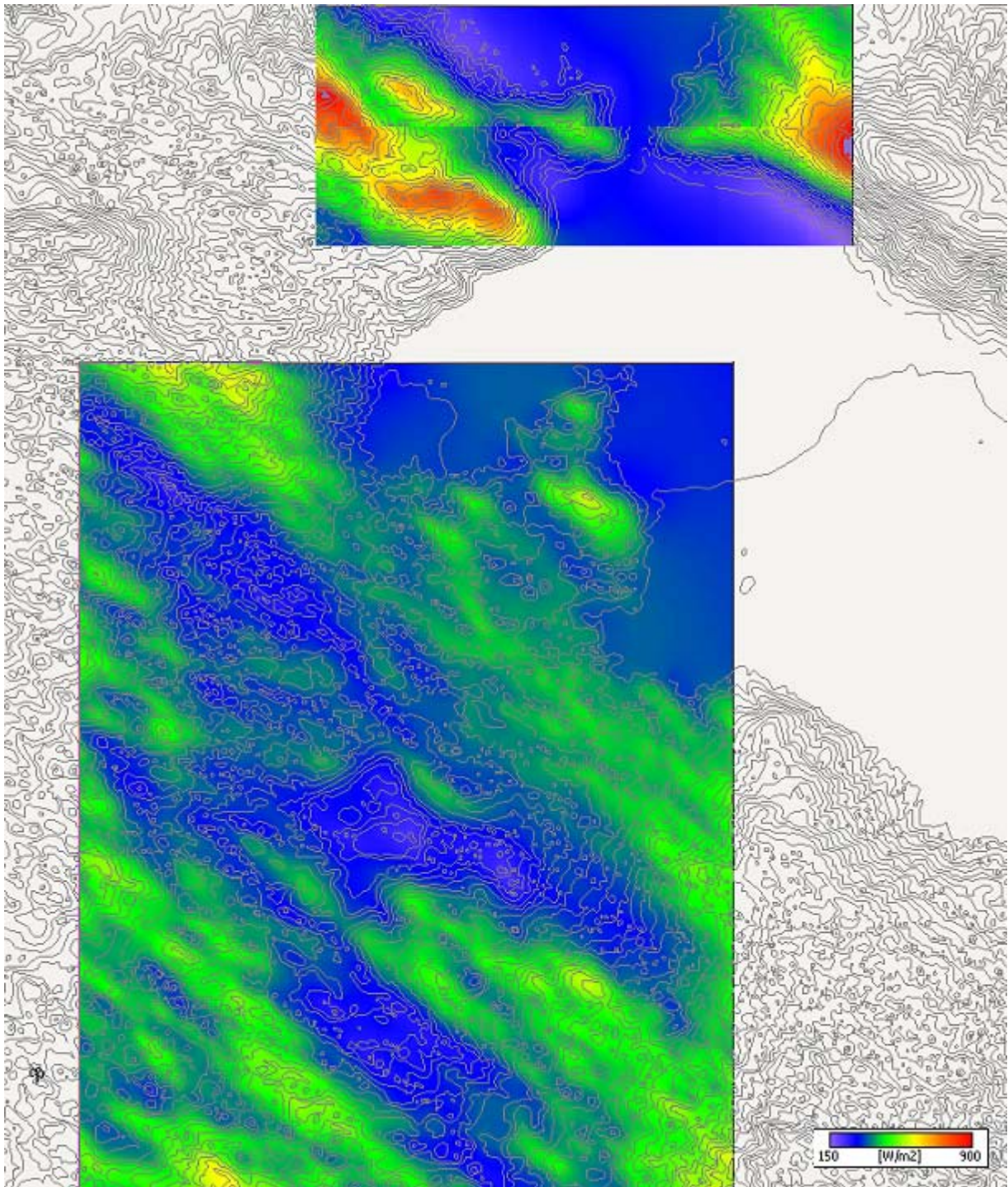


Figure 4-3 Wind energy distribution over the planned wind farm area (WAsP)

Table 4-1 Site specific conditions used in energy yield and fatigue load calculation

| | |
|------------------------------|-------|
| WF Kupres | |
| Site reference ID | MS1 |
| Annual mean temperature (°C) | 10,2 |
| Site reference height (m) | 1160 |
| Site reference air density | 1,085 |

Layout is designed considering:

- Wind turbine number optimization, restricting the minimum wind turbine production to approximately 90% of average wind farm production.
- Wind turbine position optimization, performed by the criteria of maximum energy production after every change in number of wind turbines.

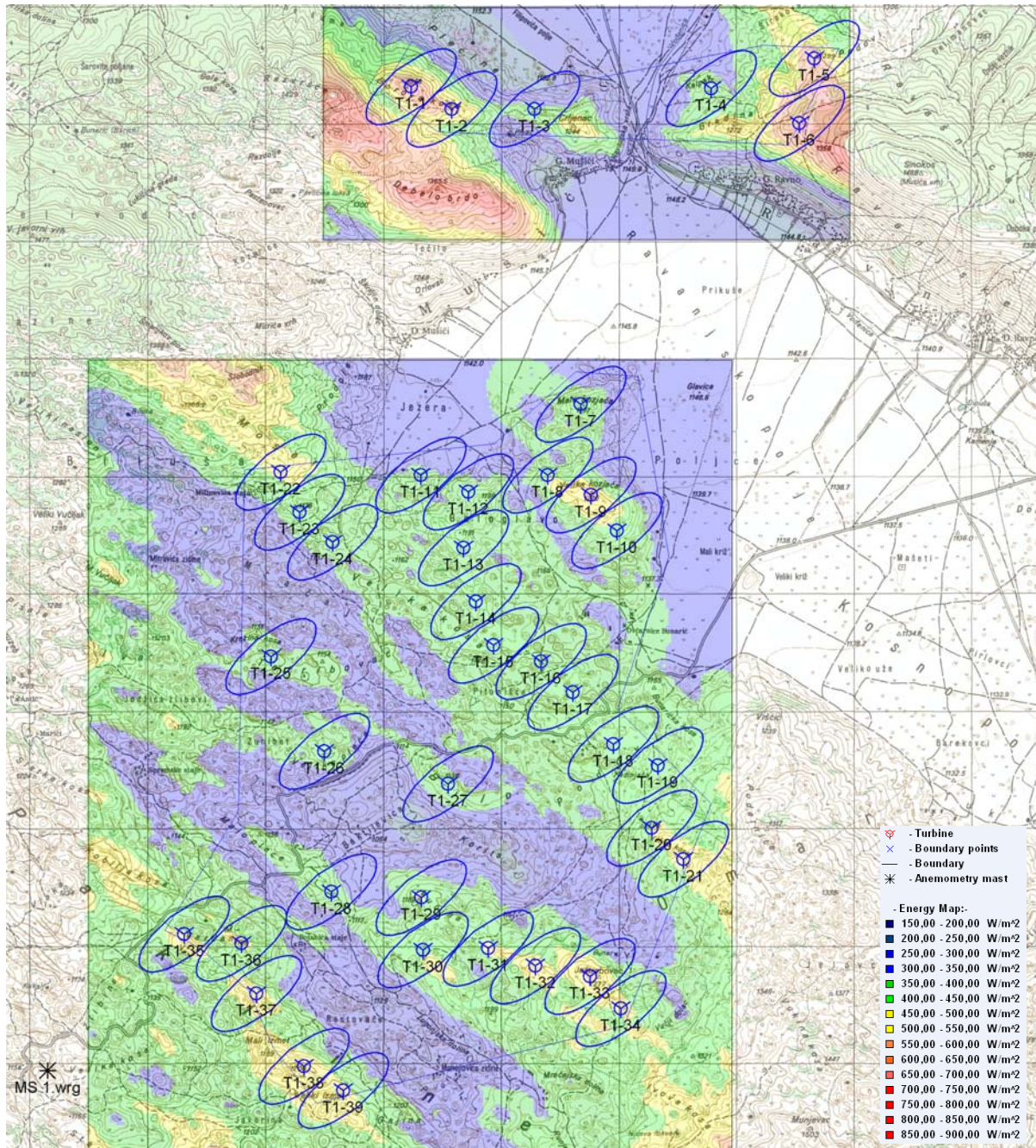


Figure 4-4 Turbine positions with separation distances and wind energy distribution over the planned wind farm area

Table 4-2 Wind turbines and measurement masts positions and altitudes

| WT/MS | X (Northing) | Y (Easting) | Altitude (m) |
|-------|--------------|-------------|--------------|
| T1-1 | 4.858.303 | 6.443.245 | 1340 |
| T1-2 | 4.858.110 | 6.443.592 | 1297 |
| T1-3 | 4.858.110 | 6.444.294 | 1207 |
| T1-4 | 4.858.286 | 6.445.799 | 1196 |
| T1-5 | 4.858.541 | 6.446.675 | 1299 |
| T1-6 | 4.857.992 | 6.446.549 | 1317 |
| T1-7 | 4.855.598 | 6.444.689 | 1189 |
| T1-8 | 4.854.996 | 6.444.407 | 1179 |
| T1-9 | 4.854.825 | 6.444.777 | 1219 |
| T1-10 | 4.854.524 | 6.444.995 | 1174 |
| T1-11 | 4.854.996 | 6.443.327 | 1151 |
| T1-12 | 4.854.853 | 6.443.734 | 1179 |
| T1-13 | 4.854.377 | 6.443.691 | 1180 |
| T1-14 | 4.853.920 | 6.443.798 | 1170 |
| T1-15 | 4.853.549 | 6.443.946 | 1160 |
| T1-16 | 4.853.409 | 6.444.353 | 1152 |
| T1-17 | 4.853.146 | 6.444.621 | 1160 |
| T1-18 | 4.852.705 | 6.444.965 | 1160 |
| T1-19 | 4.852.525 | 6.445.344 | 1173 |
| T1-20 | 4.851.991 | 6.445.292 | 1206 |
| T1-21 | 4.851.727 | 6.445.564 | 1249 |
| T1-22 | 4.855.021 | 6.442.137 | 1217 |
| T1-23 | 4.854.679 | 6.442.299 | 1170 |
| T1-24 | 4.854.424 | 6.442.579 | 1149 |
| T1-25 | 4.853.451 | 6.442.054 | 1150 |
| T1-26 | 4.852.646 | 6.442.508 | 1149 |
| T1-27 | 4.852.366 | 6.443.561 | 1130 |
| T1-28 | 4.851.449 | 6.442.569 | 1118 |
| T1-29 | 4.851.401 | 6.443.331 | 1159 |
| T1-30 | 4.850.953 | 6.443.346 | 1170 |
| T1-31 | 4.850.970 | 6.443.902 | 1190 |
| T1-32 | 4.850.818 | 6.444.302 | 1235 |
| T1-33 | 4.850.727 | 6.444.769 | 1270 |
| T1-34 | 4.850.453 | 6.445.030 | 1269 |
| T1-35 | 4.851.090 | 6.441.314 | 1162 |
| T1-36 | 4.851.008 | 6.441.801 | 1159 |
| T1-37 | 4.850.583 | 6.441.928 | 1161 |
| T1-38 | 4.849.964 | 6.442.333 | 1200 |
| T1-39 | 4.849.757 | 6.442.669 | 1210 |
| MS1 | 4.849.928 | 6.440.154 | 1160 |
| MS2 | 4.848.320 | 6.441.171 | 1225 |



Table 4-3 Energy per turbine

| No. | Gross energy (GWh) | Wake losses (%) | Net energy (GWh) | Capacity factor (%) | Net energy - index (%) |
|-------|--------------------|-----------------|------------------|---------------------|------------------------|
| T1-1 | 7,937 | 1,0 | 7,862 | 39,0 | 100 |
| T1-2 | 7,257 | 1,6 | 7,142 | 35,4 | 91 |
| T1-3 | 5,737 | 1,6 | 5,643 | 28,0 | 72 |
| T1-4 | 6,017 | 2,8 | 5,846 | 29,0 | 74 |
| T1-5 | 7,616 | 2,2 | 7,452 | 37,0 | 95 |
| T1-6 | 7,629 | 1,7 | 7,497 | 37,2 | 95 |
| T1-7 | 6,605 | 4,5 | 6,306 | 31,3 | 80 |
| T1-8 | 6,471 | 4,6 | 6,172 | 30,6 | 79 |
| T1-9 | 7,486 | 3,4 | 7,235 | 35,9 | 92 |
| T1-10 | 6,513 | 3,1 | 6,308 | 31,3 | 80 |
| T1-11 | 5,969 | 4,6 | 5,696 | 28,3 | 72 |
| T1-12 | 6,501 | 6,9 | 6,052 | 30,0 | 77 |
| T1-13 | 6,389 | 7,6 | 5,905 | 29,3 | 75 |
| T1-14 | 6,409 | 5,8 | 6,036 | 29,9 | 77 |
| T1-15 | 6,371 | 4,6 | 6,080 | 30,2 | 77 |
| T1-16 | 6,292 | 3,5 | 6,072 | 30,1 | 77 |
| T1-17 | 6,400 | 2,6 | 6,231 | 30,9 | 79 |
| T1-18 | 6,299 | 2,3 | 6,154 | 30,5 | 78 |
| T1-19 | 6,287 | 3,0 | 6,100 | 30,3 | 78 |
| T1-20 | 6,604 | 2,8 | 6,417 | 31,8 | 82 |
| T1-21 | 6,825 | 2,8 | 6,630 | 32,9 | 84 |
| T1-22 | 6,924 | 2,7 | 6,739 | 33,4 | 86 |
| T1-23 | 6,350 | 4,4 | 6,071 | 30,1 | 77 |
| T1-24 | 6,124 | 8,1 | 5,628 | 27,9 | 72 |
| T1-25 | 6,000 | 6,6 | 5,603 | 27,8 | 71 |
| T1-26 | 6,200 | 6,6 | 5,789 | 28,7 | 74 |
| T1-27 | 6,293 | 6,2 | 5,901 | 29,3 | 75 |
| T1-28 | 6,144 | 6,8 | 5,725 | 28,4 | 73 |
| T1-29 | 6,672 | 6,5 | 6,240 | 31,0 | 79 |
| T1-30 | 6,484 | 6,7 | 6,049 | 30,0 | 77 |
| T1-31 | 6,674 | 5,8 | 6,287 | 31,2 | 80 |
| T1-32 | 6,986 | 5,1 | 6,630 | 32,9 | 84 |
| T1-33 | 7,334 | 3,2 | 7,102 | 35,2 | 90 |
| T1-34 | 6,767 | 2,5 | 6,596 | 32,7 | 84 |
| T1-35 | 6,766 | 5,6 | 6,385 | 31,7 | 81 |
| T1-36 | 6,684 | 8,4 | 6,120 | 30,4 | 78 |
| T1-37 | 6,829 | 7,0 | 6,352 | 31,5 | 81 |
| T1-38 | 7,018 | 7,0 | 6,524 | 32,4 | 83 |
| T1-39 | 6,818 | 7,1 | 6,335 | 31,4 | 81 |
| Avg | 6,633 | 4,6 | 6,331 | 31,4 | 81 |
| Min | 5,737 | 1,0 | 5,603 | 27,8 | 71 |
| Max | 7,937 | 8,4 | 7,862 | 39,0 | 100 |

Table 4-4 Summary data

| | |
|---------------------------------|-----------|
| WF Kupres | |
| Number of WT | 39 |
| Total net energy (GWh) | 247 |
| Average net energy per WT (GWh) | 6,331 |
| Capacity factor (%) | 31,4 |
| Min/max wake losses (%) | 1,0 - 8,4 |

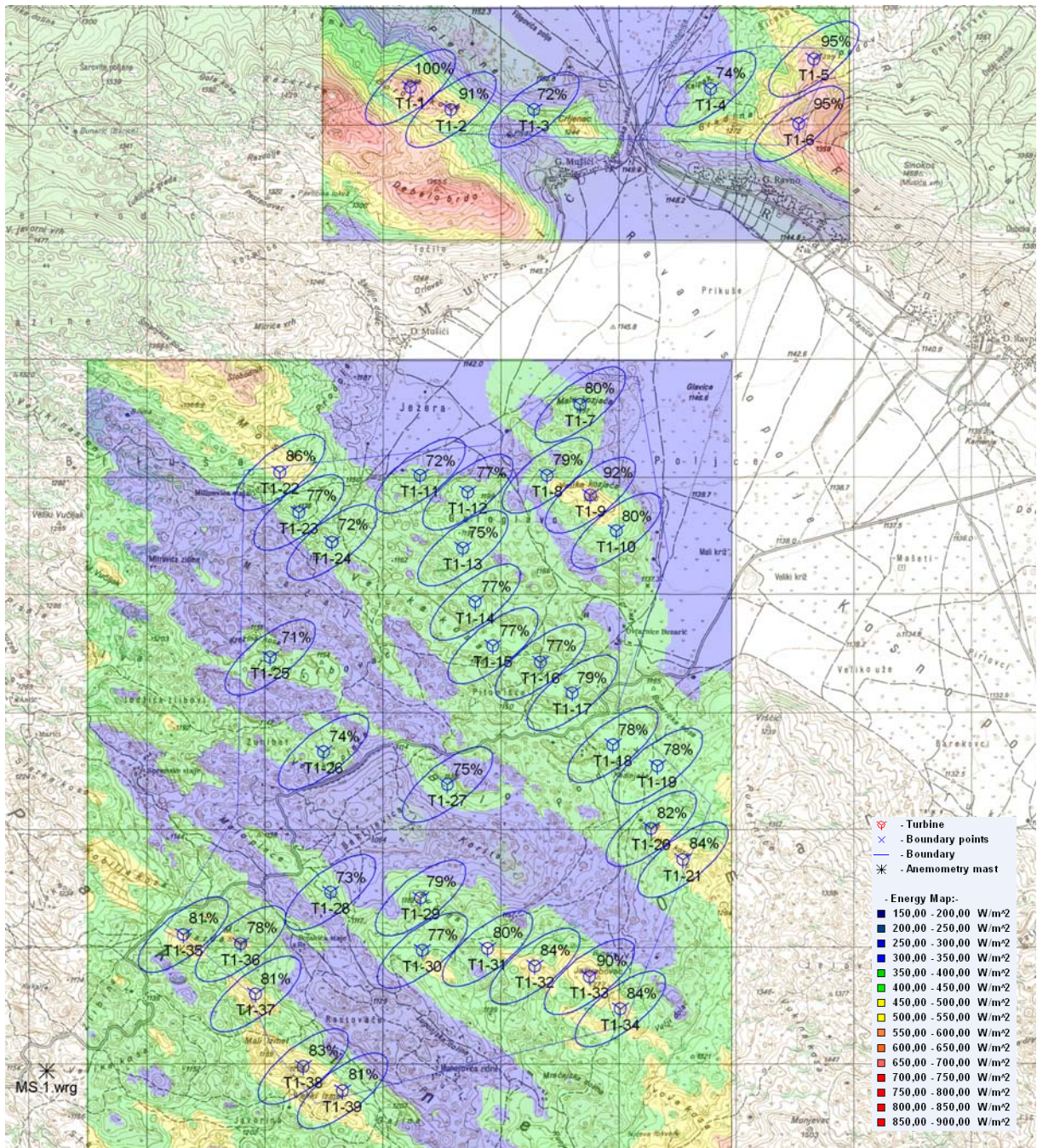


Figure 4-5 Net energy indexes

Table 4-5 Estimated design equivalent turbulence by wind speed (T1-1 - T1-10)

| v(m/s) | T1-1 | T1-2 | T1-3 | T1-4 | T1-5 | T1-6 | T1-7 | T1-8 | T1-9 | T1-10 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,186 | 0,190 | 0,173 | 0,190 | 0,150 | 0,192 | 0,186 | 0,187 | 0,180 | 0,188 |
| 5 | 0,170 | 0,191 | 0,190 | 0,190 | 0,200 | 0,178 | 0,202 | 0,206 | 0,194 | 0,194 |
| 6 | 0,161 | 0,186 | 0,169 | 0,171 | 0,185 | 0,163 | 0,190 | 0,190 | 0,189 | 0,181 |
| 7 | 0,147 | 0,170 | 0,157 | 0,158 | 0,169 | 0,151 | 0,177 | 0,177 | 0,176 | 0,168 |
| 8 | 0,137 | 0,156 | 0,149 | 0,151 | 0,155 | 0,142 | 0,166 | 0,168 | 0,165 | 0,157 |
| 9 | 0,131 | 0,146 | 0,145 | 0,148 | 0,148 | 0,136 | 0,158 | 0,160 | 0,154 | 0,148 |
| 10 | 0,125 | 0,137 | 0,139 | 0,144 | 0,142 | 0,133 | 0,152 | 0,154 | 0,144 | 0,141 |
| 11 | 0,121 | 0,130 | 0,134 | 0,139 | 0,139 | 0,131 | 0,147 | 0,147 | 0,137 | 0,136 |
| 12 | 0,118 | 0,124 | 0,134 | 0,134 | 0,136 | 0,128 | 0,142 | 0,142 | 0,130 | 0,132 |
| 13 | 0,115 | 0,118 | 0,134 | 0,136 | 0,131 | 0,124 | 0,137 | 0,137 | 0,126 | 0,129 |
| 14 | 0,111 | 0,115 | 0,131 | 0,135 | 0,127 | 0,120 | 0,133 | 0,134 | 0,122 | 0,125 |
| 15 | 0,108 | 0,116 | 0,129 | 0,132 | 0,122 | 0,120 | 0,129 | 0,131 | 0,117 | 0,122 |
| 16 | 0,109 | 0,114 | 0,126 | 0,130 | 0,123 | 0,118 | 0,126 | 0,128 | 0,114 | 0,120 |
| 17 | 0,108 | 0,111 | 0,122 | 0,127 | 0,121 | 0,116 | 0,124 | 0,125 | 0,111 | 0,118 |
| 18 | 0,104 | 0,110 | 0,120 | 0,124 | 0,118 | 0,115 | 0,122 | 0,124 | 0,109 | 0,116 |
| 19 | 0,103 | 0,108 | 0,118 | 0,122 | 0,115 | 0,113 | 0,120 | 0,124 | 0,108 | 0,115 |
| 20 | 0,102 | 0,106 | 0,117 | 0,118 | 0,112 | 0,111 | 0,118 | 0,122 | 0,107 | 0,114 |
| 21 | 0,101 | 0,104 | 0,114 | 0,114 | 0,108 | 0,110 | 0,116 | 0,120 | 0,106 | 0,112 |
| 22 | 0,103 | 0,103 | 0,104 | 0,113 | 0,104 | 0,109 | 0,116 | 0,119 | 0,104 | 0,111 |
| 23 | 0,104 | 0,102 | 0,100 | 0,111 | 0,100 | 0,108 | 0,114 | 0,114 | 0,102 | 0,110 |
| 24 | 0,104 | 0,101 | 0,097 | 0,103 | 0,099 | 0,108 | 0,108 | 0,109 | 0,101 | 0,109 |
| 25 | 0,092 | 0,077 | 0,087 | 0,037 | 0,081 | 0,106 | 0,105 | 0,095 | 0,091 | 0,108 |

Table 4-6 Estimated design equivalent turbulence by wind speed (T1-11 - T1-20)

| v(m/s) | T1-11 | T1-12 | T1-13 | T1-14 | T1-15 | T1-16 | T1-17 | T1-18 | T1-19 | T1-20 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,174 | 0,160 | 0,160 | 0,177 | 0,183 | 0,188 | 0,188 | 0,188 | 0,190 | 0,188 |
| 5 | 0,207 | 0,222 | 0,206 | 0,200 | 0,202 | 0,203 | 0,188 | 0,193 | 0,214 | 0,193 |
| 6 | 0,189 | 0,210 | 0,195 | 0,186 | 0,187 | 0,194 | 0,187 | 0,179 | 0,201 | 0,180 |
| 7 | 0,176 | 0,195 | 0,183 | 0,174 | 0,173 | 0,179 | 0,173 | 0,166 | 0,185 | 0,168 |
| 8 | 0,167 | 0,184 | 0,173 | 0,164 | 0,163 | 0,167 | 0,160 | 0,156 | 0,172 | 0,159 |
| 9 | 0,158 | 0,174 | 0,166 | 0,157 | 0,155 | 0,157 | 0,150 | 0,148 | 0,162 | 0,153 |
| 10 | 0,150 | 0,166 | 0,160 | 0,152 | 0,148 | 0,148 | 0,142 | 0,141 | 0,154 | 0,147 |
| 11 | 0,145 | 0,160 | 0,155 | 0,146 | 0,142 | 0,141 | 0,136 | 0,135 | 0,148 | 0,141 |
| 12 | 0,140 | 0,155 | 0,151 | 0,142 | 0,137 | 0,135 | 0,131 | 0,131 | 0,144 | 0,136 |
| 13 | 0,136 | 0,152 | 0,148 | 0,139 | 0,133 | 0,130 | 0,127 | 0,127 | 0,140 | 0,131 |
| 14 | 0,133 | 0,149 | 0,145 | 0,136 | 0,129 | 0,127 | 0,123 | 0,124 | 0,135 | 0,127 |
| 15 | 0,130 | 0,145 | 0,142 | 0,133 | 0,126 | 0,125 | 0,121 | 0,122 | 0,132 | 0,125 |
| 16 | 0,128 | 0,142 | 0,138 | 0,130 | 0,124 | 0,123 | 0,119 | 0,121 | 0,129 | 0,122 |
| 17 | 0,127 | 0,139 | 0,135 | 0,128 | 0,122 | 0,121 | 0,117 | 0,119 | 0,125 | 0,121 |
| 18 | 0,124 | 0,136 | 0,133 | 0,126 | 0,121 | 0,119 | 0,116 | 0,117 | 0,124 | 0,119 |
| 19 | 0,122 | 0,134 | 0,132 | 0,124 | 0,119 | 0,117 | 0,114 | 0,115 | 0,122 | 0,117 |
| 20 | 0,120 | 0,133 | 0,131 | 0,123 | 0,117 | 0,116 | 0,113 | 0,113 | 0,119 | 0,115 |
| 21 | 0,119 | 0,130 | 0,129 | 0,121 | 0,116 | 0,115 | 0,112 | 0,112 | 0,117 | 0,114 |
| 22 | 0,118 | 0,127 | 0,126 | 0,119 | 0,114 | 0,113 | 0,111 | 0,111 | 0,116 | 0,113 |
| 23 | 0,117 | 0,128 | 0,124 | 0,117 | 0,113 | 0,111 | 0,110 | 0,110 | 0,113 | 0,111 |
| 24 | 0,109 | 0,129 | 0,123 | 0,117 | 0,112 | 0,110 | 0,109 | 0,110 | 0,110 | 0,108 |
| 25 | 0,050 | 0,113 | 0,115 | 0,112 | 0,108 | 0,000 | 0,108 | 0,000 | 0,000 | 0,106 |

Table 4-7 Estimated design equivalent turbulence by wind speed (T1-21 - T1-30)

| v(m/s) | T1-21 | T1-22 | T1-23 | T1-24 | T1-25 | T1-26 | T1-27 | T1-28 | T1-29 | T1-30 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,187 | 0,177 | 0,173 | 0,169 | 0,163 | 0,138 | 0,165 | 0,139 | 0,165 | 0,122 |
| 5 | 0,193 | 0,195 | 0,194 | 0,208 | 0,192 | 0,190 | 0,198 | 0,203 | 0,205 | 0,207 |
| 6 | 0,186 | 0,181 | 0,182 | 0,198 | 0,177 | 0,175 | 0,182 | 0,184 | 0,196 | 0,186 |
| 7 | 0,173 | 0,167 | 0,169 | 0,184 | 0,166 | 0,164 | 0,170 | 0,172 | 0,182 | 0,172 |
| 8 | 0,161 | 0,156 | 0,159 | 0,172 | 0,157 | 0,155 | 0,161 | 0,162 | 0,171 | 0,163 |
| 9 | 0,150 | 0,148 | 0,152 | 0,164 | 0,150 | 0,148 | 0,154 | 0,154 | 0,161 | 0,155 |
| 10 | 0,141 | 0,142 | 0,146 | 0,157 | 0,145 | 0,143 | 0,148 | 0,148 | 0,154 | 0,149 |
| 11 | 0,135 | 0,138 | 0,140 | 0,151 | 0,140 | 0,139 | 0,144 | 0,143 | 0,149 | 0,143 |
| 12 | 0,130 | 0,134 | 0,136 | 0,147 | 0,136 | 0,135 | 0,140 | 0,138 | 0,145 | 0,136 |
| 13 | 0,126 | 0,131 | 0,131 | 0,144 | 0,133 | 0,132 | 0,136 | 0,134 | 0,143 | 0,131 |
| 14 | 0,122 | 0,128 | 0,129 | 0,141 | 0,130 | 0,129 | 0,133 | 0,131 | 0,141 | 0,127 |
| 15 | 0,119 | 0,125 | 0,126 | 0,138 | 0,128 | 0,127 | 0,131 | 0,128 | 0,138 | 0,125 |
| 16 | 0,117 | 0,122 | 0,125 | 0,136 | 0,126 | 0,125 | 0,129 | 0,126 | 0,134 | 0,122 |
| 17 | 0,115 | 0,119 | 0,123 | 0,134 | 0,124 | 0,123 | 0,126 | 0,125 | 0,130 | 0,120 |
| 18 | 0,113 | 0,117 | 0,120 | 0,131 | 0,123 | 0,121 | 0,125 | 0,123 | 0,127 | 0,118 |
| 19 | 0,112 | 0,114 | 0,118 | 0,129 | 0,121 | 0,119 | 0,123 | 0,121 | 0,125 | 0,117 |
| 20 | 0,111 | 0,114 | 0,117 | 0,127 | 0,120 | 0,118 | 0,121 | 0,119 | 0,126 | 0,116 |
| 21 | 0,109 | 0,113 | 0,116 | 0,126 | 0,118 | 0,117 | 0,120 | 0,118 | 0,124 | 0,113 |
| 22 | 0,108 | 0,110 | 0,114 | 0,125 | 0,117 | 0,116 | 0,119 | 0,117 | 0,118 | 0,111 |
| 23 | 0,107 | 0,108 | 0,114 | 0,125 | 0,115 | 0,115 | 0,118 | 0,116 | 0,118 | 0,111 |
| 24 | 0,106 | 0,108 | 0,114 | 0,125 | 0,103 | 0,113 | 0,117 | 0,115 | 0,118 | 0,109 |
| 25 | 0,074 | 0,104 | 0,112 | 0,105 | 0,093 | 0,103 | 0,107 | 0,094 | 0,108 | 0,105 |

Table 4-8 Estimated design equivalent turbulence by wind speed (T1-31 - T1-39)

| v(m/s) | T1-31 | T1-32 | T1-33 | T1-34 | T1-35 | T1-36 | T1-37 | T1-38 | T1-39 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,168 | 0,170 | 0,181 | 0,187 | 0,163 | 0,160 | 0,151 | 0,162 | 0,167 |
| 5 | 0,213 | 0,200 | 0,186 | 0,190 | 0,203 | 0,206 | 0,208 | 0,204 | 0,196 |
| 6 | 0,192 | 0,196 | 0,183 | 0,184 | 0,188 | 0,199 | 0,201 | 0,195 | 0,195 |
| 7 | 0,178 | 0,181 | 0,171 | 0,171 | 0,173 | 0,185 | 0,186 | 0,181 | 0,181 |
| 8 | 0,167 | 0,169 | 0,160 | 0,159 | 0,162 | 0,175 | 0,175 | 0,168 | 0,168 |
| 9 | 0,157 | 0,158 | 0,151 | 0,148 | 0,153 | 0,165 | 0,166 | 0,156 | 0,156 |
| 10 | 0,147 | 0,148 | 0,142 | 0,140 | 0,146 | 0,157 | 0,159 | 0,148 | 0,148 |
| 11 | 0,140 | 0,140 | 0,135 | 0,133 | 0,140 | 0,151 | 0,154 | 0,140 | 0,141 |
| 12 | 0,135 | 0,134 | 0,129 | 0,128 | 0,134 | 0,147 | 0,150 | 0,134 | 0,135 |
| 13 | 0,130 | 0,129 | 0,124 | 0,124 | 0,130 | 0,144 | 0,147 | 0,129 | 0,131 |
| 14 | 0,127 | 0,125 | 0,120 | 0,121 | 0,126 | 0,141 | 0,143 | 0,125 | 0,127 |
| 15 | 0,125 | 0,122 | 0,117 | 0,118 | 0,124 | 0,138 | 0,138 | 0,122 | 0,124 |
| 16 | 0,123 | 0,120 | 0,115 | 0,116 | 0,121 | 0,135 | 0,136 | 0,120 | 0,121 |
| 17 | 0,122 | 0,118 | 0,113 | 0,115 | 0,119 | 0,132 | 0,131 | 0,119 | 0,118 |
| 18 | 0,119 | 0,116 | 0,112 | 0,113 | 0,117 | 0,130 | 0,127 | 0,118 | 0,117 |
| 19 | 0,116 | 0,114 | 0,111 | 0,112 | 0,115 | 0,127 | 0,126 | 0,116 | 0,116 |
| 20 | 0,114 | 0,112 | 0,110 | 0,110 | 0,114 | 0,126 | 0,125 | 0,113 | 0,114 |
| 21 | 0,113 | 0,110 | 0,107 | 0,109 | 0,112 | 0,124 | 0,121 | 0,111 | 0,113 |
| 22 | 0,112 | 0,109 | 0,106 | 0,108 | 0,111 | 0,121 | 0,119 | 0,110 | 0,111 |
| 23 | 0,111 | 0,108 | 0,105 | 0,107 | 0,110 | 0,120 | 0,118 | 0,108 | 0,109 |
| 24 | 0,109 | 0,107 | 0,104 | 0,106 | 0,109 | 0,120 | 0,115 | 0,107 | 0,108 |
| 25 | 0,104 | 0,101 | 0,102 | 0,104 | 0,108 | 0,119 | 0,110 | 0,106 | 0,106 |

Table 4-9 Summary turbulence data (15m/s)

| WF Kupres | | |
|-----------|-------------|---------------|
| | WT position | I_{15_eff} |
| Min | 1 | 0,108 |
| Max | 12 | 0,145 |
| Avrg | | 0,127 |

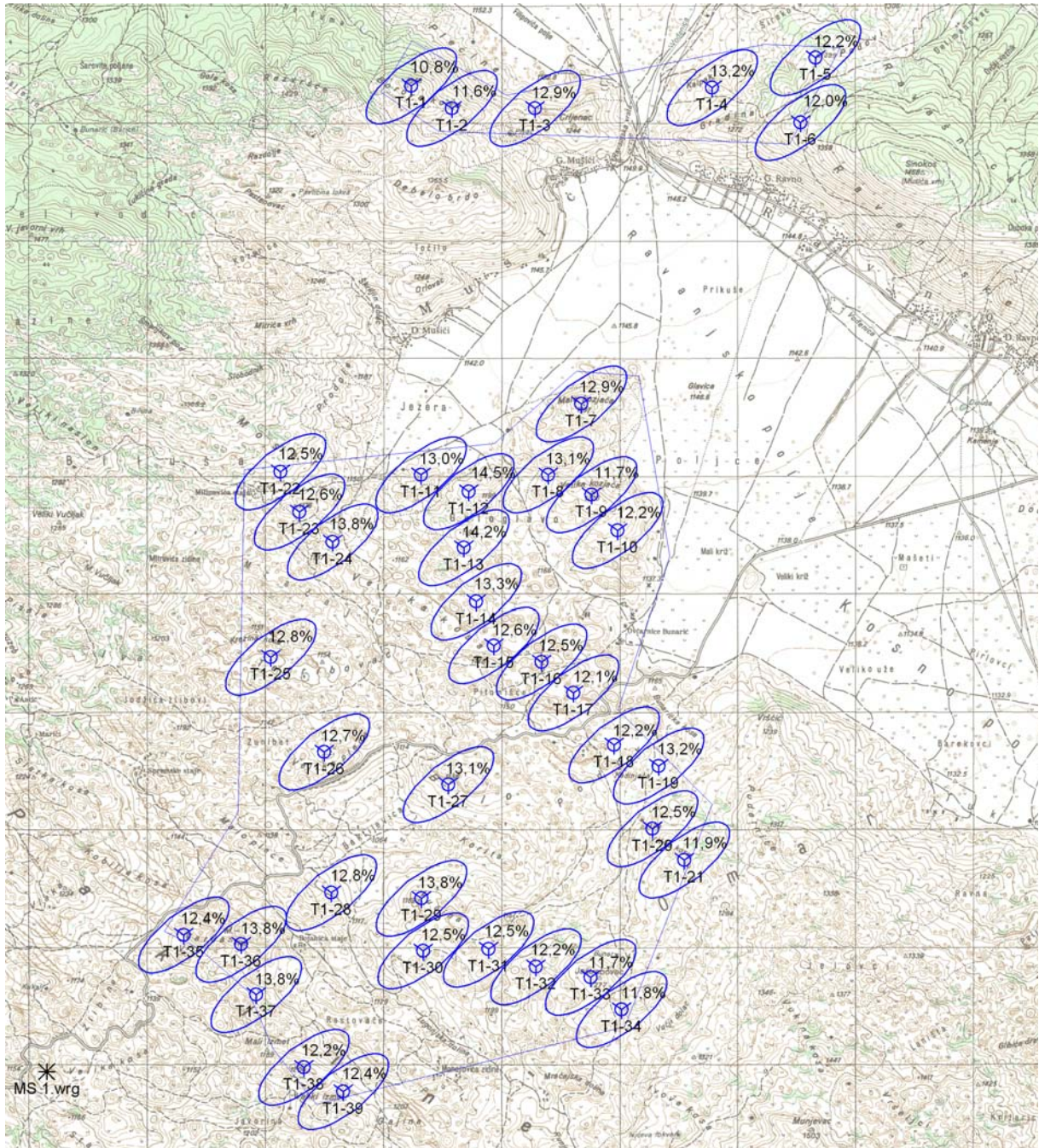


Figure 4-6 Estimated design equivalent turbulence (I_{15_eff}) according to IEC 61400-1 Ed2 standard

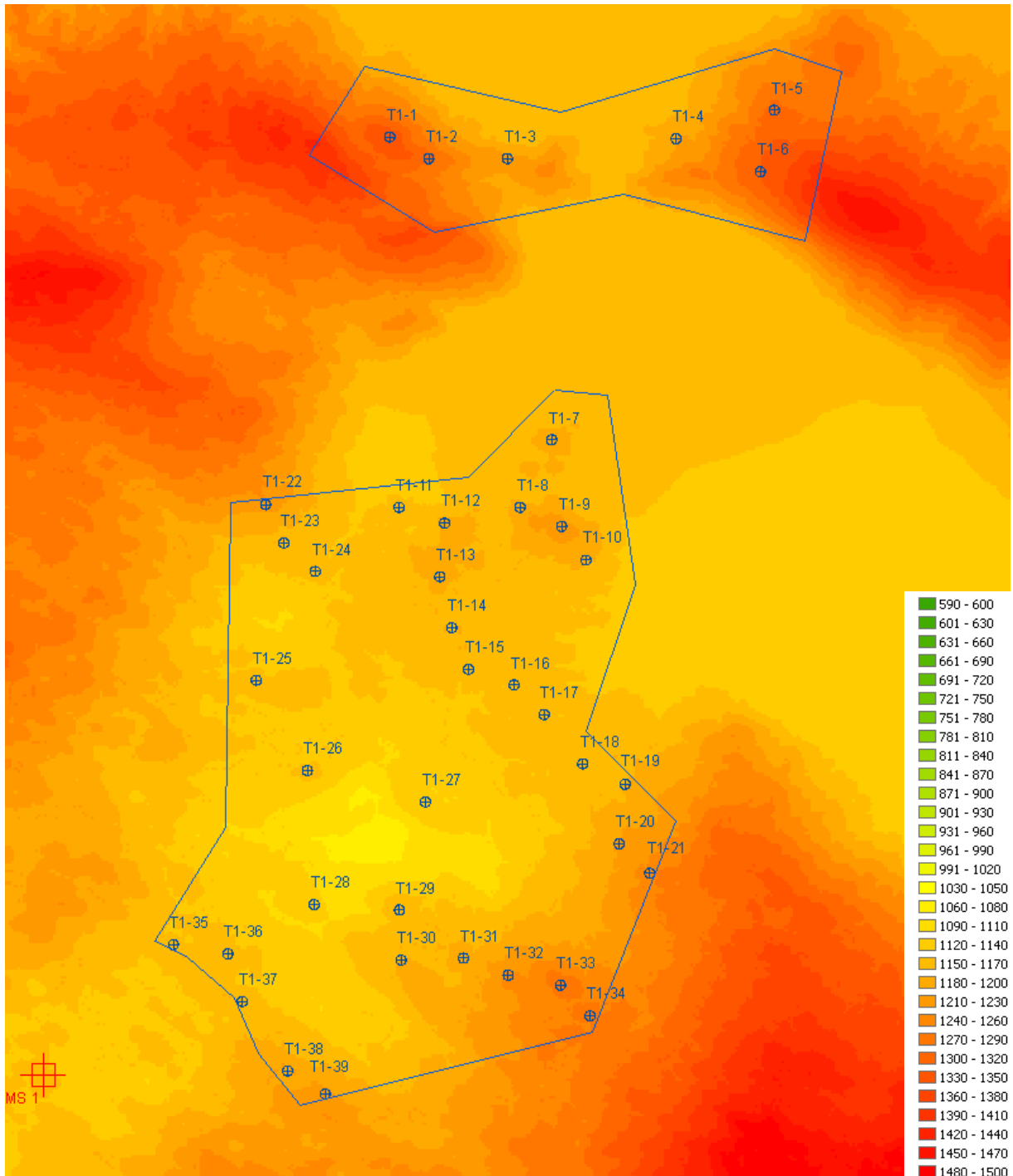


Figure 4-7 Wind turbine positions on height graduated map

5. WIND FARM PAKLINE LAYOUT

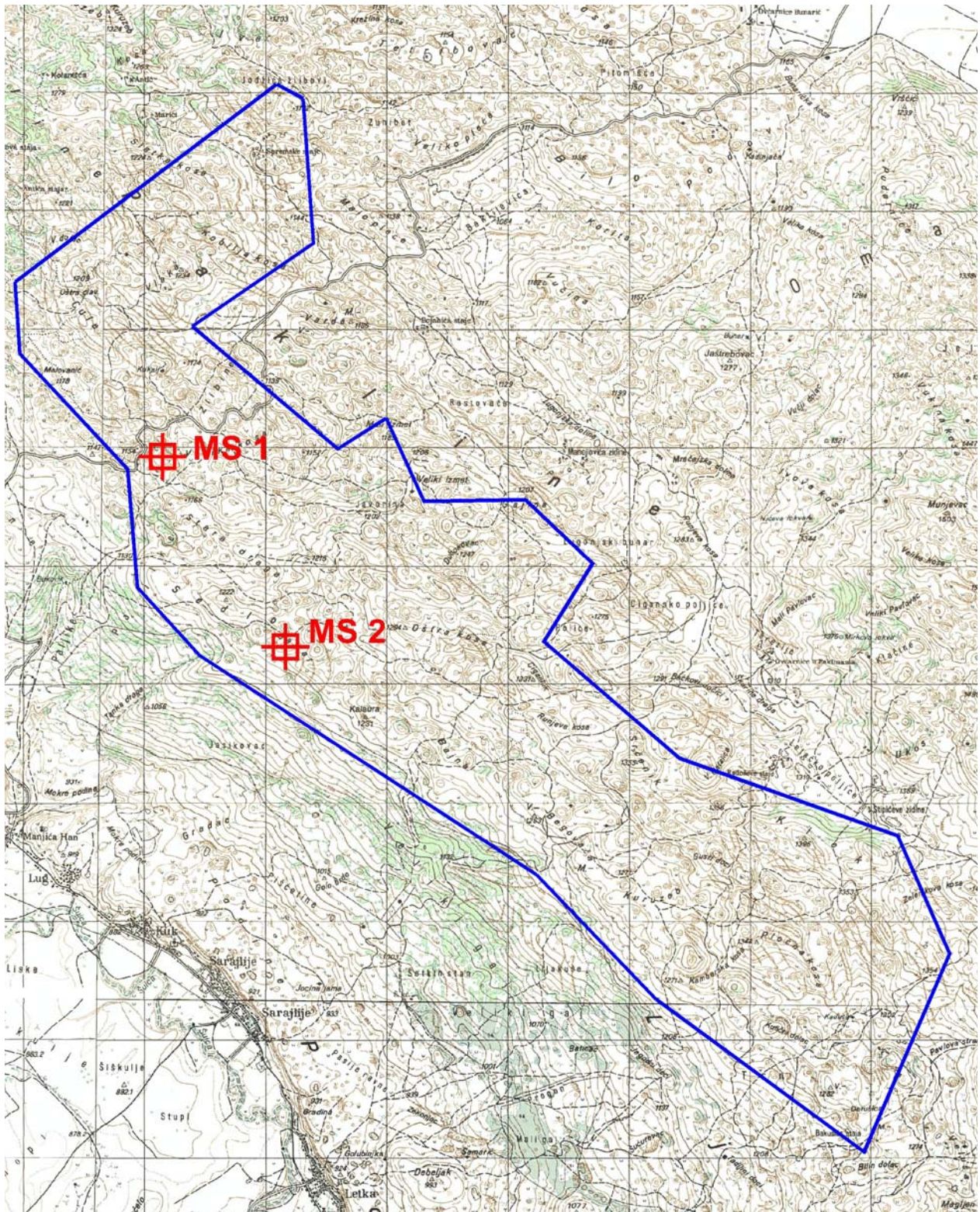


Figure 5-1 Topography map with planned wind farm area and mast position

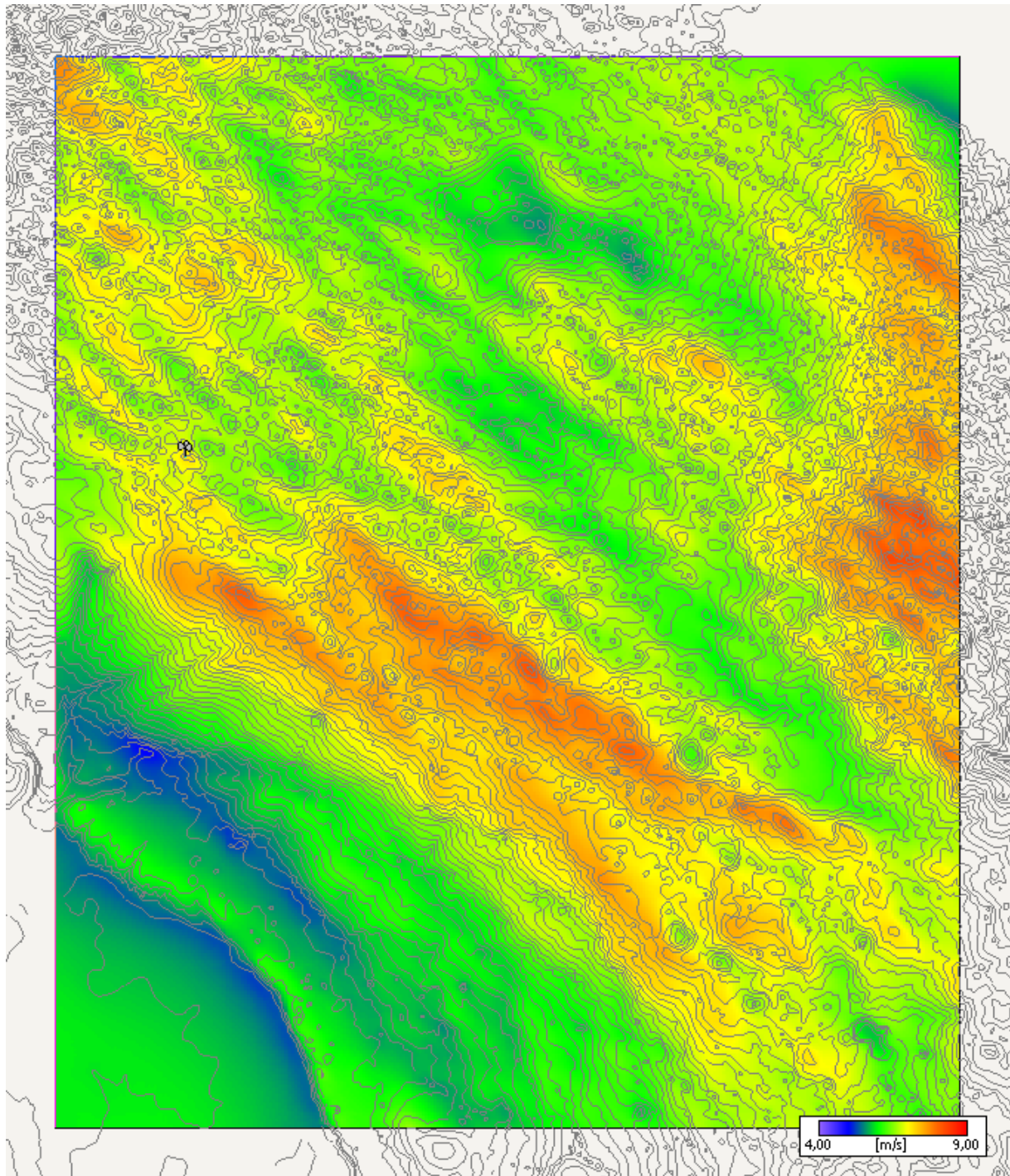


Figure 5-2 Wind speed distribution over the planned wind farm area (WAsP)

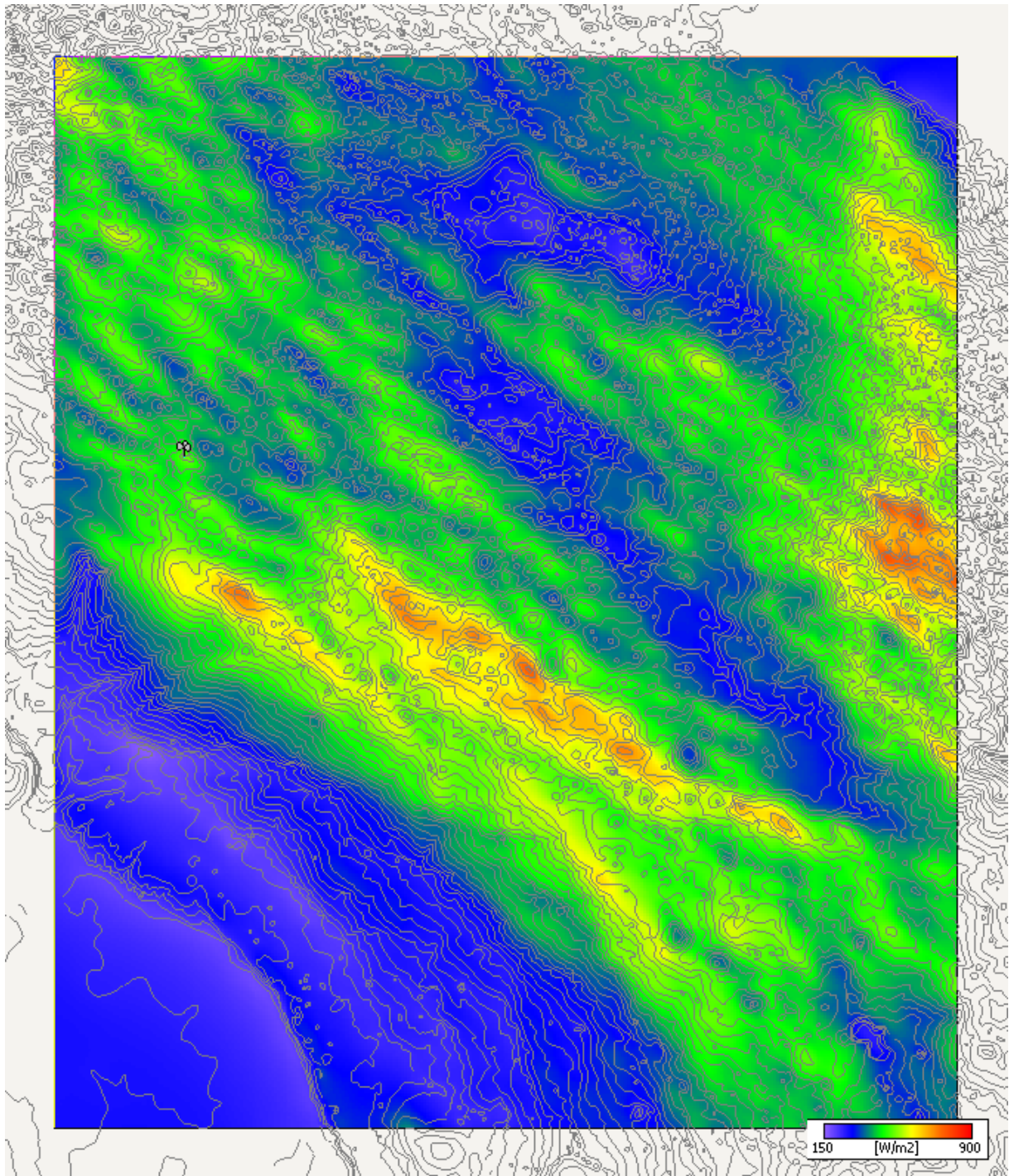


Figure 5-3 Wind energy distribution over the planned wind farm area (WASP)

Table 5-1 – Site specific conditions used in energy yield and fatigue load calculation

| | |
|------------------------------|-------|
| WF Pakline | |
| Site reference ID | MS1 |
| Annual mean temperature (°C) | 10,2 |
| Site reference height (m) | 1160 |
| Site reference air density | 1,085 |

Layout is designed considering:

- Wind turbine number optimization, restricting the minimum wind turbine production to approximately 90% of average wind farm production, but also considering the high energy of this site maximally using the available area..
- Wind turbine position optimization, performed by the criteria of maximum energy production after every change in number of wind turbines.

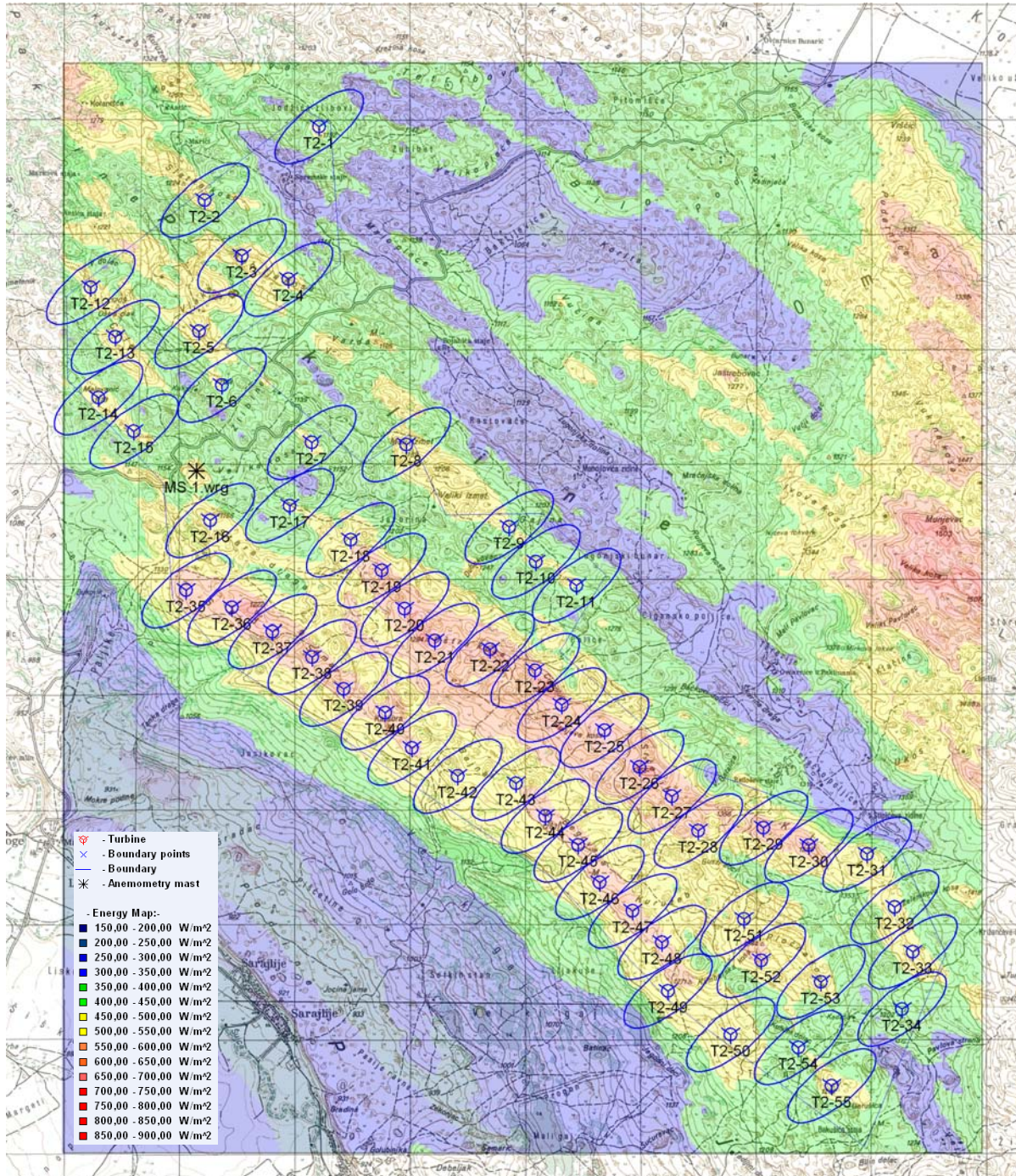


Figure 5-4 Turbine positions with separation distances and wind energy distribution over the planned wind farm area

Table 5-2 Wind turbines and measurement masts positions and altitudes

| WT/MS | X (Northing) | Y (Easting) | Altitude (m) |
|-------|--------------|-------------|--------------|
| T2-1 | 4.852.923 | 6.441.219 | 1189 |
| T2-2 | 4.852.283 | 6.440.224 | 1200 |
| T2-3 | 4.851.800 | 6.440.546 | 1216 |
| T2-4 | 4.851.595 | 6.440.951 | 1189 |
| T2-5 | 4.851.142 | 6.440.175 | 1206 |
| T2-6 | 4.850.675 | 6.440.375 | 1162 |
| T2-7 | 4.850.174 | 6.441.156 | 1160 |
| T2-8 | 4.850.158 | 6.441.978 | 1181 |
| T2-9 | 4.849.439 | 6.442.869 | 1213 |
| T2-10 | 4.849.135 | 6.443.102 | 1236 |
| T2-11 | 4.848.931 | 6.443.452 | 1250 |
| T2-12 | 4.851.526 | 6.439.235 | 1200 |
| T2-13 | 4.851.095 | 6.439.448 | 1197 |
| T2-14 | 4.850.566 | 6.439.304 | 1169 |
| T2-15 | 4.850.271 | 6.439.611 | 1150 |
| T2-16 | 4.849.497 | 6.440.274 | 1160 |
| T2-17 | 4.849.622 | 6.440.964 | 1150 |
| T2-18 | 4.849.328 | 6.441.491 | 1209 |
| T2-19 | 4.849.062 | 6.441.764 | 1246 |
| T2-20 | 4.848.727 | 6.441.963 | 1271 |
| T2-21 | 4.848.454 | 6.442.222 | 1290 |
| T2-22 | 4.848.377 | 6.442.704 | 1309 |
| T2-23 | 4.848.195 | 6.443.094 | 1305 |
| T2-24 | 4.847.896 | 6.443.325 | 1310 |
| T2-25 | 4.847.673 | 6.443.696 | 1330 |
| T2-26 | 4.847.355 | 6.444.001 | 1349 |
| T2-27 | 4.847.100 | 6.444.284 | 1330 |
| T2-28 | 4.846.800 | 6.444.511 | 1330 |
| T2-29 | 4.846.827 | 6.445.078 | 1379 |
| T2-30 | 4.846.671 | 6.445.472 | 1389 |
| T2-31 | 4.846.597 | 6.445.976 | 1390 |
| T2-32 | 4.846.135 | 6.446.218 | 1379 |
| T2-33 | 4.845.748 | 6.446.376 | 1370 |
| T2-34 | 4.845.249 | 6.446.283 | 1320 |
| T2-35 | 4.848.888 | 6.440.064 | 1170 |
| T2-36 | 4.848.738 | 6.440.461 | 1198 |
| T2-37 | 4.848.532 | 6.440.815 | 1205 |
| T2-38 | 4.848.313 | 6.441.157 | 1220 |
| T2-39 | 4.848.034 | 6.441.431 | 1216 |
| T2-40 | 4.847.826 | 6.441.793 | 1230 |
| T2-41 | 4.847.520 | 6.442.025 | 1215 |
| T2-42 | 4.847.275 | 6.442.422 | 1219 |
| T2-43 | 4.847.212 | 6.442.930 | 1250 |
| T2-44 | 4.846.929 | 6.443.182 | 1260 |
| T2-45 | 4.846.675 | 6.443.467 | 1260 |
| T2-46 | 4.846.351 | 6.443.656 | 1260 |
| T2-47 | 4.846.104 | 6.443.943 | 1266 |
| T2-48 | 4.845.829 | 6.444.198 | 1269 |
| T2-49 | 4.845.404 | 6.444.247 | 1239 |
| T2-50 | 4.845.028 | 6.444.794 | 1258 |
| T2-51 | 4.846.033 | 6.444.910 | 1319 |
| T2-52 | 4.845.672 | 6.445.060 | 1328 |
| T2-53 | 4.845.484 | 6.445.577 | 1330 |
| T2-54 | 4.844.913 | 6.445.382 | 1270 |
| T2-55 | 4.844.581 | 6.445.670 | 1280 |
| MS1 | 4.849.928 | 6.440.154 | 1160 |
| MS2 | 4.848.320 | 6.441.171 | 1225 |

Table 5-3 Energy per turbine

| No. | Gross energy (GWh) | Wake losses (%) | Net energy (GWh) | Capacity factor (%) | Net energy - index (%) |
|-------|--------------------|-----------------|------------------|---------------------|------------------------|
| T2-1 | 6,717 | 6,9 | 6,251 | 31,0 | 80 |
| T2-2 | 6,658 | 5,6 | 6,283 | 31,2 | 80 |
| T2-3 | 7,098 | 5,8 | 6,689 | 33,2 | 86 |
| T2-4 | 6,920 | 5,9 | 6,512 | 32,3 | 83 |
| T2-5 | 7,041 | 7,3 | 6,530 | 32,4 | 84 |
| T2-6 | 6,716 | 5,9 | 6,320 | 31,3 | 81 |
| T2-7 | 6,829 | 9,6 | 6,173 | 30,6 | 79 |
| T2-8 | 6,946 | 7,4 | 6,432 | 31,9 | 82 |
| T2-9 | 6,628 | 6,1 | 6,223 | 30,9 | 80 |
| T2-10 | 6,610 | 5,6 | 6,240 | 31,0 | 80 |
| T2-11 | 6,578 | 5,1 | 6,244 | 31,0 | 80 |
| T2-12 | 6,909 | 3,7 | 6,651 | 33,0 | 85 |
| T2-13 | 6,930 | 6,6 | 6,471 | 32,1 | 83 |
| T2-14 | 6,927 | 5,2 | 6,570 | 32,6 | 84 |
| T2-15 | 6,832 | 5,6 | 6,449 | 32,0 | 83 |
| T2-16 | 7,049 | 7,5 | 6,517 | 32,3 | 83 |
| T2-17 | 6,649 | 8,3 | 6,100 | 30,3 | 78 |
| T2-18 | 7,119 | 8,4 | 6,519 | 32,3 | 84 |
| T2-19 | 7,596 | 8,1 | 6,980 | 34,6 | 89 |
| T2-20 | 7,931 | 7,5 | 7,339 | 36,4 | 94 |
| T2-21 | 8,021 | 7,9 | 7,386 | 36,6 | 95 |
| T2-22 | 8,008 | 6,2 | 7,515 | 37,3 | 96 |
| T2-23 | 7,896 | 3,6 | 7,612 | 37,8 | 98 |
| T2-24 | 7,844 | 3,6 | 7,562 | 37,5 | 97 |
| T2-25 | 7,825 | 3,6 | 7,544 | 37,4 | 97 |
| T2-26 | 8,106 | 3,7 | 7,807 | 38,7 | 100 |
| T2-27 | 7,710 | 3,4 | 7,449 | 37,0 | 95 |
| T2-28 | 7,346 | 3,9 | 7,057 | 35,0 | 90 |
| T2-29 | 7,822 | 3,3 | 7,566 | 37,5 | 97 |
| T2-30 | 7,836 | 3,8 | 7,537 | 37,4 | 97 |
| T2-31 | 6,978 | 2,9 | 6,777 | 33,6 | 87 |
| T2-32 | 6,863 | 3,5 | 6,624 | 32,9 | 85 |
| T2-33 | 7,007 | 3,4 | 6,766 | 33,6 | 87 |
| T2-34 | 6,293 | 3,9 | 6,051 | 30,0 | 78 |
| T2-35 | 7,563 | 5,1 | 7,176 | 35,6 | 92 |
| T2-36 | 7,746 | 4,7 | 7,378 | 36,6 | 95 |
| T2-37 | 7,648 | 4,5 | 7,303 | 36,2 | 94 |
| T2-38 | 7,632 | 5,4 | 7,216 | 35,8 | 92 |
| T2-39 | 7,521 | 5,7 | 7,092 | 35,2 | 91 |
| T2-40 | 7,487 | 5,2 | 7,096 | 35,2 | 91 |
| T2-41 | 7,374 | 4,3 | 7,060 | 35,0 | 90 |
| T2-42 | 7,145 | 4,7 | 6,806 | 33,8 | 87 |
| T2-43 | 7,149 | 4,5 | 6,825 | 33,9 | 87 |
| T2-44 | 7,409 | 3,9 | 7,118 | 35,3 | 91 |
| T2-45 | 7,374 | 4,1 | 7,070 | 35,1 | 91 |
| T2-46 | 7,508 | 4,9 | 7,142 | 35,4 | 91 |
| T2-47 | 7,528 | 4,6 | 7,182 | 35,6 | 92 |
| T2-48 | 7,415 | 6,0 | 6,972 | 34,6 | 89 |
| T2-49 | 7,196 | 5,6 | 6,790 | 33,7 | 87 |
| T2-50 | 6,999 | 5,9 | 6,588 | 32,7 | 84 |
| T2-51 | 7,094 | 5,4 | 6,710 | 33,3 | 86 |
| T2-52 | 7,359 | 6,3 | 6,898 | 34,2 | 88 |
| T2-53 | 7,080 | 7,8 | 6,525 | 32,4 | 84 |
| T2-54 | 6,606 | 6,6 | 6,168 | 30,6 | 79 |
| T2-55 | 6,909 | 3,6 | 6,658 | 33,0 | 85 |
| Avg | 7,236 | 5,4 | 6,846 | 34,0 | 88 |
| Min | 6,293 | 2,9 | 6,051 | 30,0 | 78 |
| Max | 8,106 | 9,6 | 7,807 | 38,7 | 100 |

Table 5-4 Summary data

| | |
|---------------------------------|-----------|
| WF Pakline | |
| Number of WT | 55 |
| Total net energy (GWh) | 377 |
| Average net energy per WT (GWh) | 6,846 |
| Capacity factor (%) | 34,0 |
| Min/max wake losses (%) | 2,9 - 9,6 |

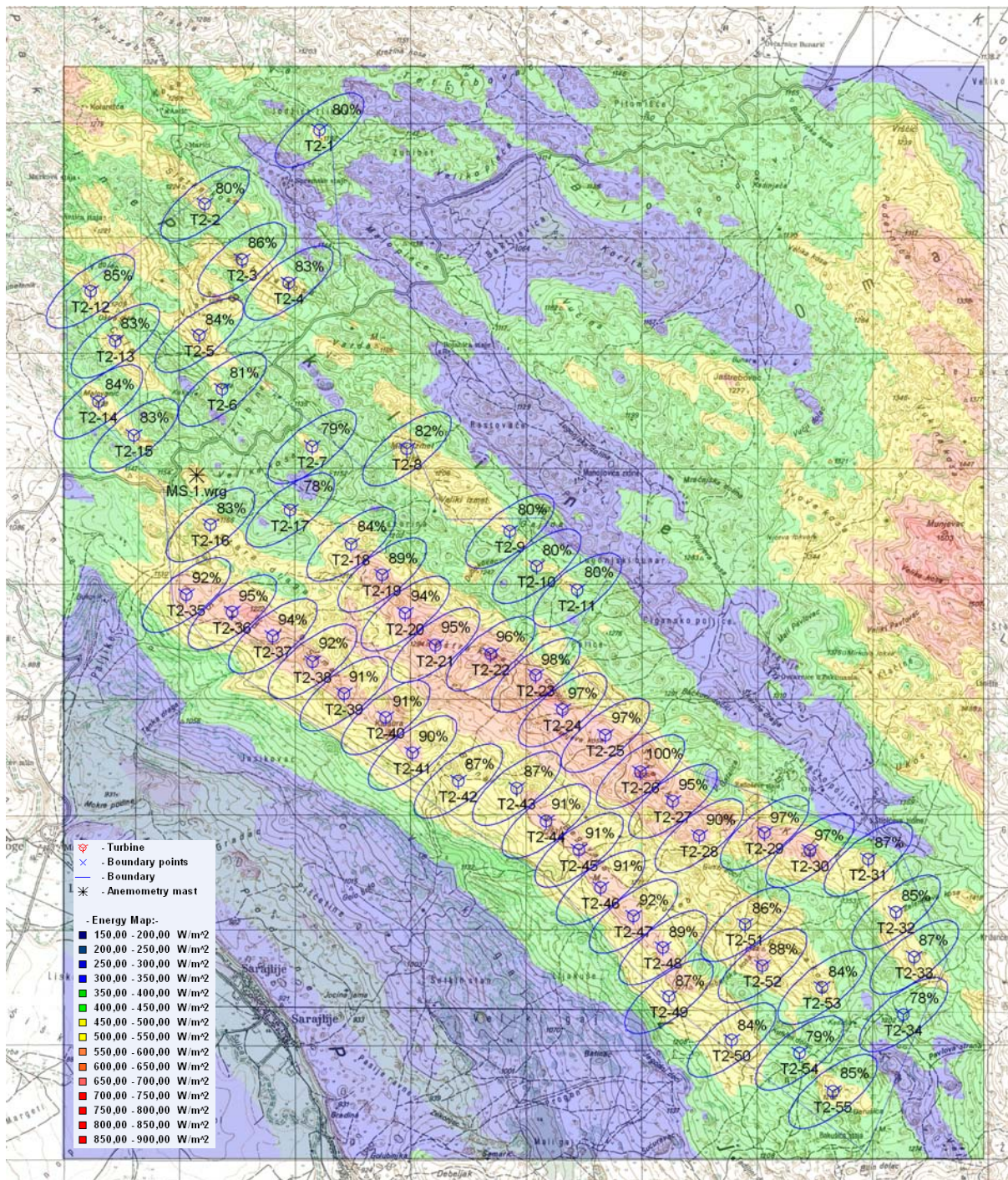


Figure 5-5 Net energy indexes

Table 5-5 Estimated design equivalent turbulence by wind speed (T2-1 – T2-10)

| v(m/s) | T2-1 | T2-2 | T2-3 | T2-4 | T2-5 | T2-6 | T2-7 | T2-8 | T2-9 | T2-10 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,160 | 0,167 | 0,152 | 0,139 | 0,172 | 0,182 | 0,151 | 0,160 | 0,171 | 0,177 |
| 5 | 0,190 | 0,187 | 0,188 | 0,193 | 0,200 | 0,192 | 0,214 | 0,193 | 0,193 | 0,197 |
| 6 | 0,175 | 0,170 | 0,178 | 0,180 | 0,183 | 0,176 | 0,196 | 0,180 | 0,177 | 0,183 |
| 7 | 0,161 | 0,154 | 0,163 | 0,164 | 0,168 | 0,161 | 0,180 | 0,166 | 0,160 | 0,168 |
| 8 | 0,152 | 0,145 | 0,150 | 0,150 | 0,157 | 0,151 | 0,168 | 0,156 | 0,149 | 0,156 |
| 9 | 0,146 | 0,139 | 0,144 | 0,141 | 0,151 | 0,145 | 0,161 | 0,150 | 0,142 | 0,148 |
| 10 | 0,144 | 0,137 | 0,138 | 0,135 | 0,147 | 0,142 | 0,157 | 0,146 | 0,138 | 0,143 |
| 11 | 0,140 | 0,134 | 0,137 | 0,131 | 0,144 | 0,139 | 0,153 | 0,141 | 0,135 | 0,139 |
| 12 | 0,136 | 0,130 | 0,132 | 0,126 | 0,139 | 0,134 | 0,148 | 0,133 | 0,130 | 0,133 |
| 13 | 0,132 | 0,127 | 0,127 | 0,122 | 0,136 | 0,131 | 0,144 | 0,129 | 0,126 | 0,128 |
| 14 | 0,132 | 0,125 | 0,123 | 0,119 | 0,131 | 0,129 | 0,141 | 0,123 | 0,125 | 0,128 |
| 15 | 0,133 | 0,128 | 0,123 | 0,120 | 0,134 | 0,131 | 0,141 | 0,127 | 0,125 | 0,127 |
| 16 | 0,130 | 0,125 | 0,123 | 0,119 | 0,132 | 0,129 | 0,139 | 0,126 | 0,122 | 0,124 |
| 17 | 0,127 | 0,122 | 0,119 | 0,116 | 0,128 | 0,125 | 0,135 | 0,122 | 0,119 | 0,123 |
| 18 | 0,125 | 0,120 | 0,117 | 0,114 | 0,126 | 0,123 | 0,132 | 0,120 | 0,118 | 0,122 |
| 19 | 0,123 | 0,118 | 0,116 | 0,113 | 0,124 | 0,122 | 0,130 | 0,118 | 0,116 | 0,119 |
| 20 | 0,121 | 0,116 | 0,115 | 0,111 | 0,122 | 0,120 | 0,128 | 0,115 | 0,114 | 0,116 |
| 21 | 0,119 | 0,115 | 0,112 | 0,110 | 0,121 | 0,119 | 0,126 | 0,113 | 0,112 | 0,114 |
| 22 | 0,118 | 0,114 | 0,110 | 0,108 | 0,120 | 0,117 | 0,124 | 0,112 | 0,110 | 0,110 |
| 23 | 0,117 | 0,113 | 0,109 | 0,107 | 0,118 | 0,115 | 0,123 | 0,111 | 0,109 | 0,108 |
| 24 | 0,117 | 0,113 | 0,109 | 0,107 | 0,115 | 0,115 | 0,122 | 0,110 | 0,108 | 0,107 |
| 25 | 0,117 | 0,112 | 0,107 | 0,106 | 0,114 | 0,113 | 0,107 | 0,108 | 0,106 | 0,103 |

Table 5-6 Estimated design equivalent turbulence by wind speed (T2-11 – T2-20)

| v(m/s) | T2-11 | T2-12 | T2-13 | T2-14 | T2-15 | T2-16 | T2-17 | T2-18 | T2-19 | T2-20 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,184 | 0,191 | 0,183 | 0,191 | 0,191 | 0,178 | 0,168 | 0,159 | 0,145 | 0,161 |
| 5 | 0,200 | 0,185 | 0,215 | 0,194 | 0,193 | 0,206 | 0,203 | 0,198 | 0,196 | 0,195 |
| 6 | 0,190 | 0,167 | 0,195 | 0,180 | 0,185 | 0,188 | 0,186 | 0,185 | 0,189 | 0,183 |
| 7 | 0,174 | 0,152 | 0,179 | 0,167 | 0,170 | 0,172 | 0,171 | 0,169 | 0,174 | 0,169 |
| 8 | 0,161 | 0,141 | 0,167 | 0,158 | 0,159 | 0,160 | 0,161 | 0,157 | 0,160 | 0,155 |
| 9 | 0,151 | 0,135 | 0,159 | 0,154 | 0,151 | 0,153 | 0,156 | 0,150 | 0,150 | 0,146 |
| 10 | 0,144 | 0,132 | 0,154 | 0,151 | 0,147 | 0,148 | 0,153 | 0,145 | 0,143 | 0,140 |
| 11 | 0,138 | 0,131 | 0,151 | 0,148 | 0,144 | 0,145 | 0,149 | 0,143 | 0,139 | 0,136 |
| 12 | 0,133 | 0,126 | 0,146 | 0,142 | 0,139 | 0,141 | 0,143 | 0,138 | 0,135 | 0,133 |
| 13 | 0,128 | 0,124 | 0,141 | 0,138 | 0,136 | 0,137 | 0,139 | 0,134 | 0,130 | 0,129 |
| 14 | 0,128 | 0,120 | 0,135 | 0,134 | 0,133 | 0,133 | 0,138 | 0,129 | 0,126 | 0,125 |
| 15 | 0,126 | 0,124 | 0,136 | 0,136 | 0,136 | 0,133 | 0,138 | 0,131 | 0,123 | 0,121 |
| 16 | 0,123 | 0,123 | 0,134 | 0,134 | 0,133 | 0,132 | 0,136 | 0,130 | 0,124 | 0,122 |
| 17 | 0,121 | 0,118 | 0,130 | 0,129 | 0,129 | 0,128 | 0,132 | 0,127 | 0,122 | 0,121 |
| 18 | 0,120 | 0,117 | 0,127 | 0,126 | 0,128 | 0,125 | 0,129 | 0,124 | 0,119 | 0,119 |
| 19 | 0,118 | 0,115 | 0,124 | 0,125 | 0,125 | 0,123 | 0,128 | 0,123 | 0,117 | 0,117 |
| 20 | 0,116 | 0,113 | 0,122 | 0,124 | 0,123 | 0,121 | 0,127 | 0,120 | 0,115 | 0,115 |
| 21 | 0,114 | 0,112 | 0,120 | 0,123 | 0,122 | 0,119 | 0,126 | 0,118 | 0,113 | 0,113 |
| 22 | 0,110 | 0,111 | 0,119 | 0,122 | 0,120 | 0,117 | 0,124 | 0,117 | 0,112 | 0,111 |
| 23 | 0,109 | 0,110 | 0,118 | 0,119 | 0,119 | 0,113 | 0,122 | 0,115 | 0,111 | 0,109 |
| 24 | 0,107 | 0,110 | 0,117 | 0,115 | 0,119 | 0,111 | 0,115 | 0,113 | 0,109 | 0,108 |
| 25 | 0,097 | 0,107 | 0,110 | 0,108 | 0,110 | 0,111 | 0,106 | 0,110 | 0,106 | 0,104 |

Table 5-7 Estimated design equivalent turbulence by wind speed (T2-21 – T2-30)

| v(m/s) | T2-21 | T2-22 | T2-23 | T2-24 | T2-25 | T2-26 | T2-27 | T2-28 | T2-29 | T2-30 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,145 | 0,178 | 0,171 | 0,185 | 0,185 | 0,166 | 0,183 | 0,177 | 0,184 | 0,178 |
| 5 | 0,206 | 0,199 | 0,192 | 0,192 | 0,191 | 0,187 | 0,196 | 0,206 | 0,190 | 0,198 |
| 6 | 0,197 | 0,189 | 0,187 | 0,180 | 0,186 | 0,178 | 0,187 | 0,184 | 0,183 | 0,192 |
| 7 | 0,180 | 0,174 | 0,172 | 0,165 | 0,171 | 0,164 | 0,171 | 0,167 | 0,167 | 0,174 |
| 8 | 0,166 | 0,161 | 0,157 | 0,153 | 0,156 | 0,152 | 0,156 | 0,155 | 0,154 | 0,160 |
| 9 | 0,155 | 0,152 | 0,146 | 0,143 | 0,144 | 0,141 | 0,145 | 0,146 | 0,144 | 0,150 |
| 10 | 0,146 | 0,145 | 0,137 | 0,135 | 0,136 | 0,134 | 0,137 | 0,140 | 0,137 | 0,141 |
| 11 | 0,141 | 0,139 | 0,132 | 0,130 | 0,130 | 0,129 | 0,132 | 0,134 | 0,131 | 0,135 |
| 12 | 0,136 | 0,134 | 0,127 | 0,126 | 0,125 | 0,125 | 0,127 | 0,129 | 0,125 | 0,129 |
| 13 | 0,131 | 0,130 | 0,123 | 0,122 | 0,122 | 0,121 | 0,123 | 0,124 | 0,121 | 0,124 |
| 14 | 0,126 | 0,125 | 0,119 | 0,118 | 0,117 | 0,116 | 0,118 | 0,120 | 0,116 | 0,119 |
| 15 | 0,122 | 0,122 | 0,115 | 0,115 | 0,114 | 0,112 | 0,114 | 0,120 | 0,114 | 0,115 |
| 16 | 0,122 | 0,123 | 0,113 | 0,115 | 0,113 | 0,111 | 0,113 | 0,118 | 0,114 | 0,114 |
| 17 | 0,120 | 0,121 | 0,113 | 0,114 | 0,112 | 0,110 | 0,113 | 0,116 | 0,113 | 0,113 |
| 18 | 0,118 | 0,119 | 0,112 | 0,113 | 0,110 | 0,110 | 0,110 | 0,113 | 0,111 | 0,110 |
| 19 | 0,116 | 0,118 | 0,110 | 0,109 | 0,109 | 0,108 | 0,109 | 0,112 | 0,110 | 0,109 |
| 20 | 0,114 | 0,116 | 0,107 | 0,107 | 0,107 | 0,107 | 0,107 | 0,110 | 0,108 | 0,107 |
| 21 | 0,113 | 0,113 | 0,106 | 0,106 | 0,106 | 0,104 | 0,106 | 0,109 | 0,106 | 0,105 |
| 22 | 0,111 | 0,111 | 0,105 | 0,105 | 0,104 | 0,103 | 0,104 | 0,107 | 0,104 | 0,104 |
| 23 | 0,109 | 0,110 | 0,104 | 0,104 | 0,103 | 0,101 | 0,103 | 0,105 | 0,103 | 0,102 |
| 24 | 0,108 | 0,109 | 0,103 | 0,101 | 0,101 | 0,099 | 0,101 | 0,104 | 0,101 | 0,101 |
| 25 | 0,104 | 0,105 | 0,096 | 0,094 | 0,097 | 0,096 | 0,098 | 0,102 | 0,099 | 0,099 |

Table 5-8 Estimated design equivalent turbulence by wind speed (T2-31 – T2-40)

| v(m/s) | T2-31 | T2-32 | T2-33 | T2-34 | T2-35 | T2-36 | T2-37 | T2-38 | T2-39 | T2-40 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,190 | 0,188 | 0,190 | 0,188 | 0,166 | 0,169 | 0,163 | 0,164 | 0,165 | 0,163 |
| 5 | 0,184 | 0,197 | 0,203 | 0,199 | 0,196 | 0,199 | 0,193 | 0,195 | 0,195 | 0,194 |
| 6 | 0,178 | 0,178 | 0,194 | 0,183 | 0,183 | 0,189 | 0,189 | 0,191 | 0,189 | 0,189 |
| 7 | 0,163 | 0,162 | 0,178 | 0,168 | 0,167 | 0,174 | 0,173 | 0,175 | 0,174 | 0,174 |
| 8 | 0,151 | 0,151 | 0,165 | 0,161 | 0,155 | 0,161 | 0,159 | 0,162 | 0,162 | 0,160 |
| 9 | 0,143 | 0,143 | 0,157 | 0,156 | 0,149 | 0,150 | 0,149 | 0,153 | 0,153 | 0,150 |
| 10 | 0,136 | 0,138 | 0,151 | 0,153 | 0,143 | 0,142 | 0,142 | 0,146 | 0,148 | 0,143 |
| 11 | 0,130 | 0,135 | 0,148 | 0,148 | 0,140 | 0,136 | 0,137 | 0,143 | 0,144 | 0,140 |
| 12 | 0,125 | 0,131 | 0,144 | 0,142 | 0,135 | 0,129 | 0,130 | 0,137 | 0,138 | 0,135 |
| 13 | 0,121 | 0,128 | 0,139 | 0,137 | 0,130 | 0,125 | 0,126 | 0,133 | 0,134 | 0,131 |
| 14 | 0,119 | 0,126 | 0,135 | 0,137 | 0,125 | 0,120 | 0,121 | 0,129 | 0,130 | 0,126 |
| 15 | 0,120 | 0,126 | 0,133 | 0,137 | 0,124 | 0,121 | 0,122 | 0,128 | 0,130 | 0,126 |
| 16 | 0,119 | 0,124 | 0,132 | 0,132 | 0,124 | 0,120 | 0,121 | 0,128 | 0,130 | 0,125 |
| 17 | 0,116 | 0,121 | 0,128 | 0,128 | 0,123 | 0,119 | 0,120 | 0,126 | 0,128 | 0,123 |
| 18 | 0,114 | 0,119 | 0,125 | 0,127 | 0,121 | 0,118 | 0,119 | 0,124 | 0,126 | 0,121 |
| 19 | 0,112 | 0,117 | 0,123 | 0,127 | 0,118 | 0,115 | 0,116 | 0,122 | 0,123 | 0,119 |
| 20 | 0,110 | 0,116 | 0,121 | 0,126 | 0,115 | 0,112 | 0,113 | 0,119 | 0,120 | 0,116 |
| 21 | 0,108 | 0,115 | 0,120 | 0,124 | 0,114 | 0,109 | 0,111 | 0,116 | 0,118 | 0,115 |
| 22 | 0,107 | 0,114 | 0,117 | 0,122 | 0,114 | 0,107 | 0,109 | 0,114 | 0,117 | 0,114 |
| 23 | 0,106 | 0,112 | 0,115 | 0,116 | 0,113 | 0,107 | 0,108 | 0,113 | 0,114 | 0,110 |
| 24 | 0,105 | 0,110 | 0,115 | 0,110 | 0,112 | 0,105 | 0,107 | 0,104 | 0,105 | 0,105 |
| 25 | 0,102 | 0,105 | 0,111 | 0,102 | 0,110 | 0,103 | 0,100 | 0,102 | 0,098 | 0,099 |

Table 5-9 Estimated design equivalent turbulence by wind speed (T2-41 – T2-50)

| v(m/s) | T2-41 | T2-42 | T2-43 | T2-44 | T2-45 | T2-46 | T2-47 | T2-48 | T2-49 | T2-50 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,168 | 0,174 | 0,170 | 0,173 | 0,172 | 0,169 | 0,169 | 0,169 | 0,190 | 0,187 |
| 5 | 0,188 | 0,199 | 0,199 | 0,199 | 0,203 | 0,192 | 0,196 | 0,207 | 0,192 | 0,201 |
| 6 | 0,174 | 0,188 | 0,187 | 0,187 | 0,192 | 0,180 | 0,190 | 0,200 | 0,178 | 0,183 |
| 7 | 0,160 | 0,170 | 0,172 | 0,172 | 0,177 | 0,166 | 0,175 | 0,184 | 0,165 | 0,167 |
| 8 | 0,148 | 0,158 | 0,161 | 0,160 | 0,163 | 0,154 | 0,160 | 0,169 | 0,155 | 0,157 |
| 9 | 0,141 | 0,150 | 0,153 | 0,151 | 0,153 | 0,147 | 0,149 | 0,160 | 0,150 | 0,151 |
| 10 | 0,135 | 0,144 | 0,147 | 0,145 | 0,147 | 0,141 | 0,141 | 0,153 | 0,146 | 0,147 |
| 11 | 0,132 | 0,139 | 0,143 | 0,142 | 0,143 | 0,139 | 0,137 | 0,150 | 0,144 | 0,145 |
| 12 | 0,128 | 0,134 | 0,138 | 0,136 | 0,138 | 0,135 | 0,132 | 0,146 | 0,137 | 0,139 |
| 13 | 0,124 | 0,129 | 0,134 | 0,132 | 0,134 | 0,131 | 0,127 | 0,142 | 0,134 | 0,136 |
| 14 | 0,120 | 0,125 | 0,130 | 0,128 | 0,130 | 0,127 | 0,123 | 0,140 | 0,130 | 0,132 |
| 15 | 0,121 | 0,127 | 0,131 | 0,128 | 0,128 | 0,125 | 0,119 | 0,137 | 0,131 | 0,133 |
| 16 | 0,121 | 0,126 | 0,130 | 0,128 | 0,129 | 0,127 | 0,122 | 0,137 | 0,131 | 0,132 |
| 17 | 0,119 | 0,123 | 0,127 | 0,126 | 0,127 | 0,125 | 0,121 | 0,135 | 0,128 | 0,128 |
| 18 | 0,117 | 0,120 | 0,125 | 0,124 | 0,124 | 0,123 | 0,117 | 0,130 | 0,125 | 0,125 |
| 19 | 0,115 | 0,118 | 0,122 | 0,122 | 0,122 | 0,121 | 0,115 | 0,126 | 0,123 | 0,124 |
| 20 | 0,113 | 0,116 | 0,120 | 0,119 | 0,120 | 0,118 | 0,113 | 0,124 | 0,121 | 0,122 |
| 21 | 0,111 | 0,114 | 0,118 | 0,117 | 0,118 | 0,116 | 0,112 | 0,124 | 0,119 | 0,121 |
| 22 | 0,110 | 0,113 | 0,117 | 0,115 | 0,116 | 0,114 | 0,111 | 0,122 | 0,118 | 0,120 |
| 23 | 0,107 | 0,108 | 0,115 | 0,115 | 0,114 | 0,113 | 0,110 | 0,118 | 0,116 | 0,117 |
| 24 | 0,101 | 0,103 | 0,106 | 0,103 | 0,111 | 0,111 | 0,108 | 0,116 | 0,115 | 0,115 |
| 25 | 0,099 | 0,098 | 0,097 | 0,098 | 0,102 | 0,108 | 0,105 | 0,114 | 0,108 | 0,115 |

Table 5-10 Estimated design equivalent turbulence by wind speed (T2-51 – T2-55)

| v(m/s) | T2-51 | T2-52 | T2-53 | T2-54 | T2-55 |
|--------|-------|-------|-------|-------|-------|
| 4 | 0,181 | 0,173 | 0,183 | 0,185 | 0,190 |
| 5 | 0,204 | 0,204 | 0,214 | 0,199 | 0,189 |
| 6 | 0,185 | 0,187 | 0,195 | 0,184 | 0,179 |
| 7 | 0,170 | 0,171 | 0,179 | 0,170 | 0,164 |
| 8 | 0,158 | 0,158 | 0,167 | 0,161 | 0,152 |
| 9 | 0,151 | 0,150 | 0,159 | 0,155 | 0,145 |
| 10 | 0,146 | 0,145 | 0,154 | 0,152 | 0,141 |
| 11 | 0,144 | 0,142 | 0,151 | 0,148 | 0,139 |
| 12 | 0,139 | 0,138 | 0,146 | 0,143 | 0,133 |
| 13 | 0,135 | 0,134 | 0,142 | 0,138 | 0,131 |
| 14 | 0,131 | 0,129 | 0,137 | 0,137 | 0,126 |
| 15 | 0,132 | 0,127 | 0,138 | 0,138 | 0,129 |
| 16 | 0,131 | 0,127 | 0,136 | 0,135 | 0,128 |
| 17 | 0,128 | 0,125 | 0,133 | 0,131 | 0,123 |
| 18 | 0,125 | 0,121 | 0,130 | 0,129 | 0,121 |
| 19 | 0,123 | 0,119 | 0,128 | 0,127 | 0,119 |
| 20 | 0,121 | 0,118 | 0,126 | 0,126 | 0,118 |
| 21 | 0,120 | 0,116 | 0,124 | 0,125 | 0,117 |
| 22 | 0,119 | 0,114 | 0,122 | 0,123 | 0,115 |
| 23 | 0,115 | 0,112 | 0,121 | 0,119 | 0,114 |
| 24 | 0,110 | 0,111 | 0,120 | 0,118 | 0,112 |
| 25 | 0,108 | 0,109 | 0,116 | 0,114 | 0,110 |

Table 5-11 Summary turbulence data (15m/s)

| WF Pakline | | |
|------------|-------------|---------------|
| | WT position | I_{15_eff} |
| Min | 26 | 0,112 |
| Max | 7 | 0,141 |
| Avrg | | 0,127 |

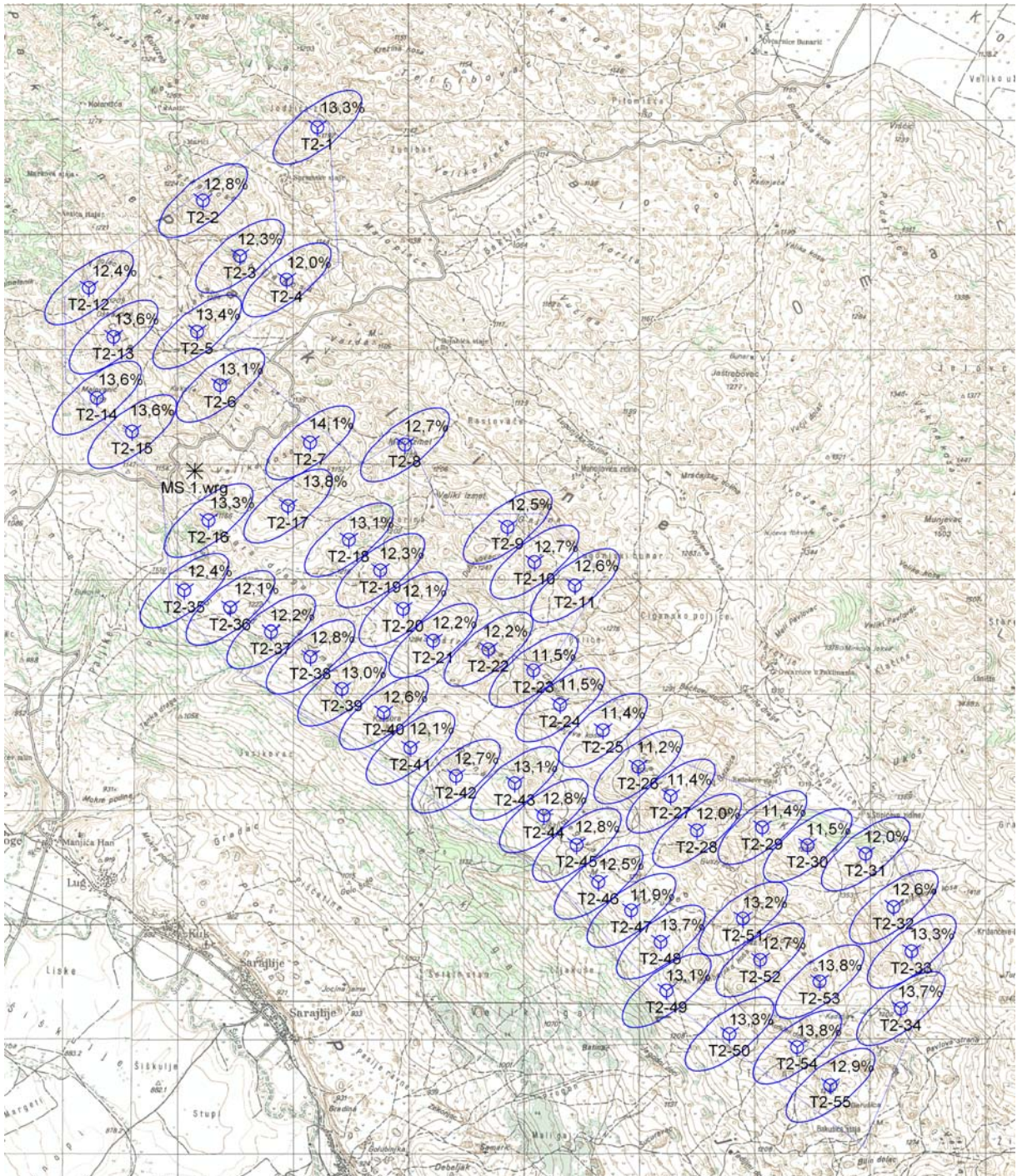


Figure 5-6 Estimated design equivalent turbulence (I_{15_eff}) according to IEC 61400-1 Ed2 standard

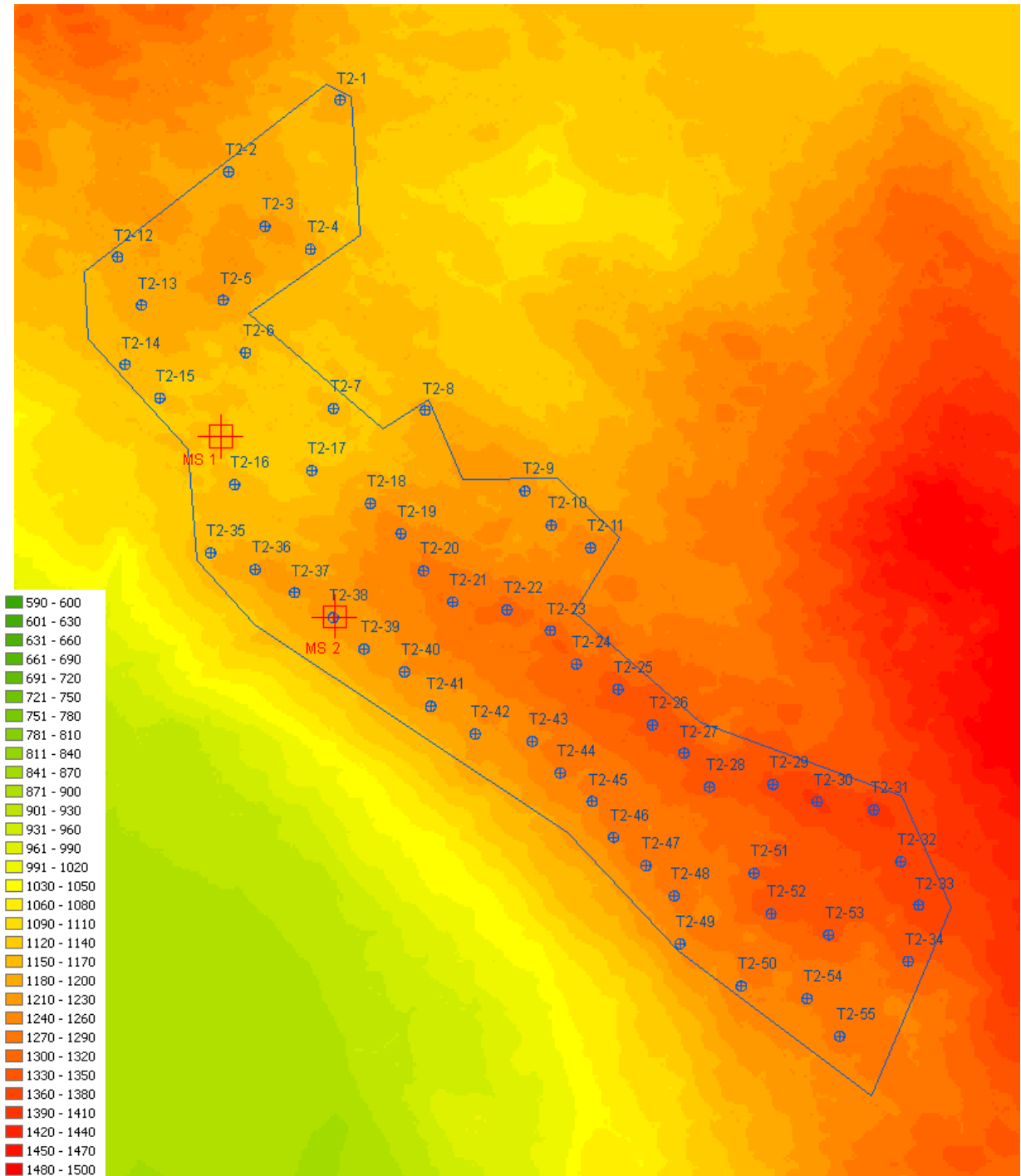


Figure 5-7 Wind turbine positions on height graduated map

6. WIND FARM LJUBUSA LAYOUT

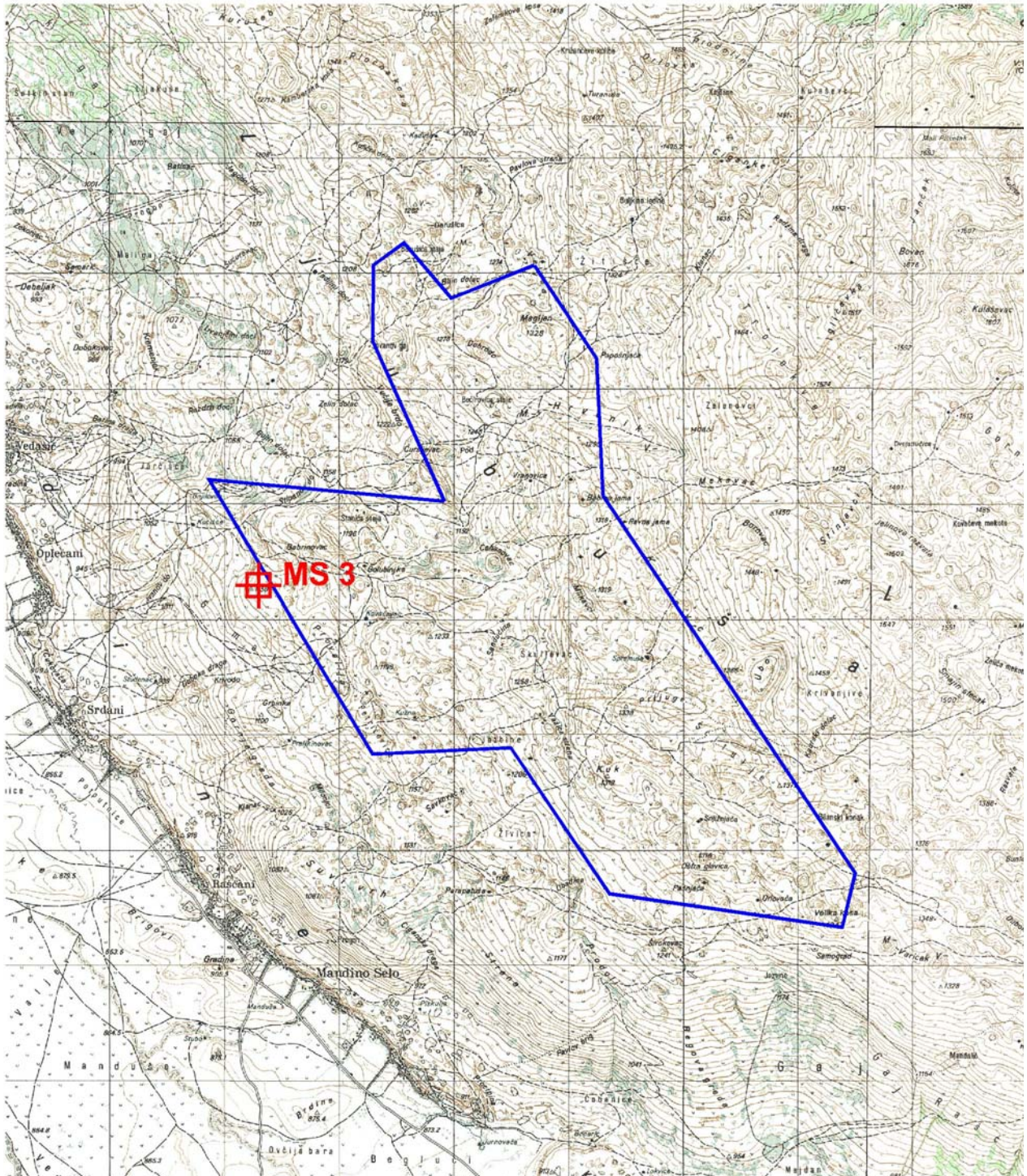


Figure 6-1 Topography map with planned wind farm area and mast position

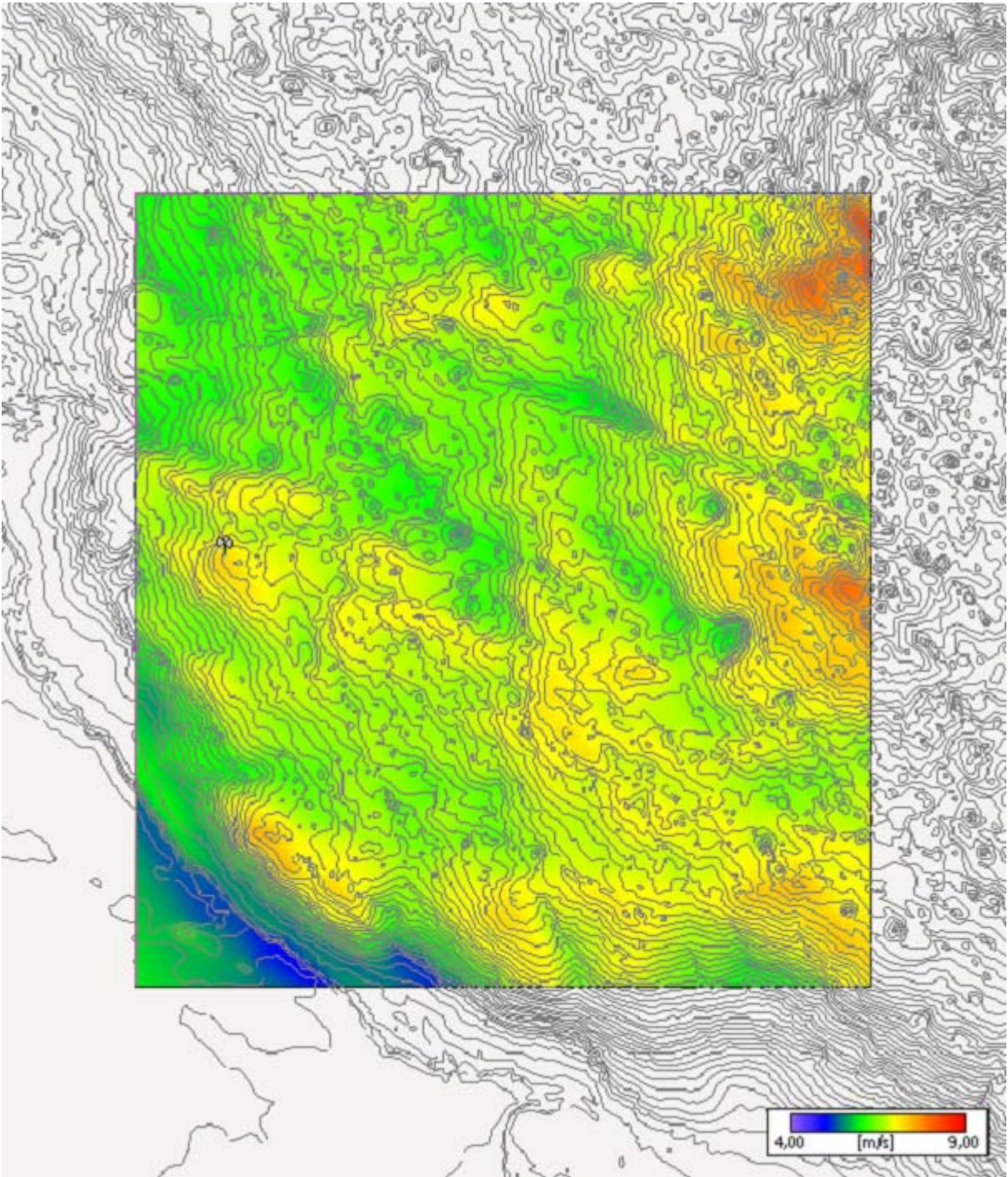


Figure 6-2 Wind speed distribution over the planed wind farm area (WAsP)

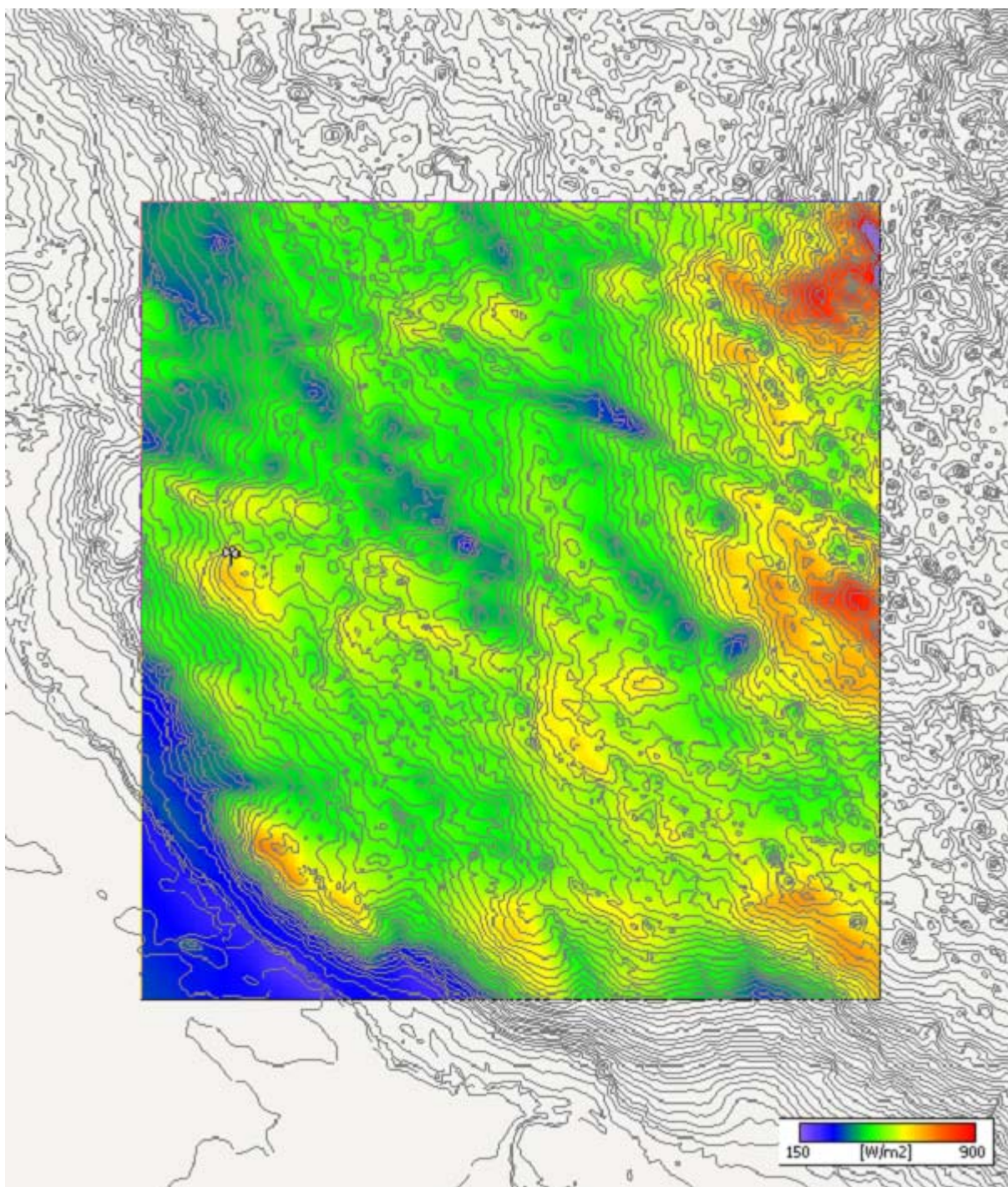


Figure 6-3 Wind energy distribution over the planned wind farm area (WAsP)

Table 6-1 Site specific conditions used in energy yield and fatigue load calculation

| | |
|------------------------------|-------|
| WF Ljubusa | |
| Site reference ID | MS3 |
| Annual mean temperature (°C) | 10,2 |
| Site reference height (m) | 1160 |
| Site reference air density | 1,085 |

Layout is designed considering:

- Wind turbine number optimization, restricting the minimum wind turbine production to approximately 90% of average wind farm production. Considering the high turbulence intensity observed on this site, number and layout of turbines was optimized to stay within wind turbine manufacturer limits.
- Wind turbine position optimization, performed by the criteria of maximum energy production after every change in number of wind turbines.

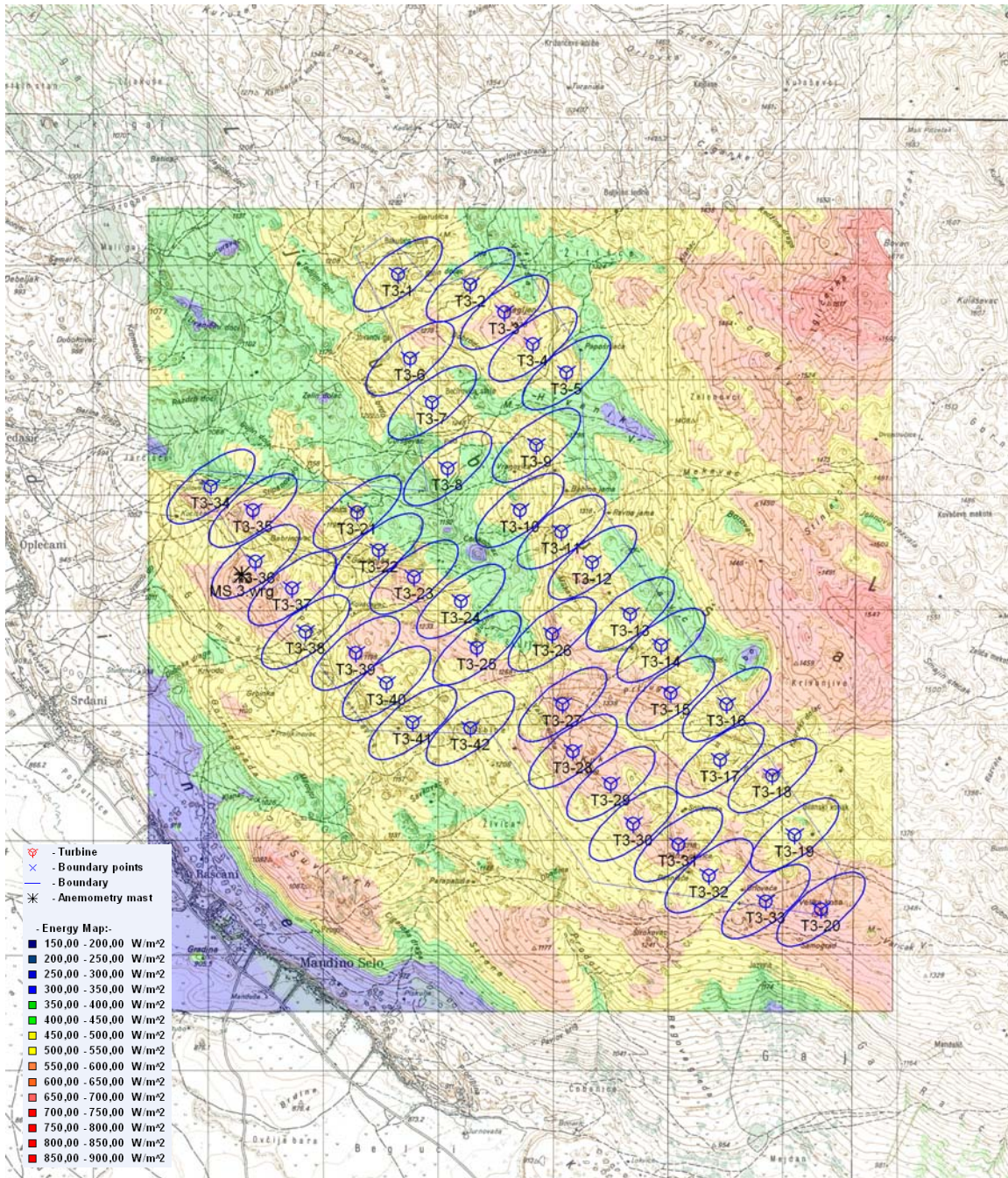


Figure 6-4 Turbine positions with separation distances and wind energy distribution over the planned wind farm area

Table 6-2 Wind turbines and measurement masts positions and altitudes

| WT/MS | X (Northing) | Y (Easting) | Altitude (m) |
|-------|--------------|-------------|--------------|
| T3-1 | 4.843.908 | 6.445.671 | 1249 |
| T3-2 | 4.843.818 | 6.446.299 | 1282 |
| T3-3 | 4.843.578 | 6.446.597 | 1319 |
| T3-4 | 4.843.298 | 6.446.844 | 1319 |
| T3-5 | 4.843.052 | 6.447.136 | 1310 |
| T3-6 | 4.843.174 | 6.445.774 | 1249 |
| T3-7 | 4.842.794 | 6.445.967 | 1242 |
| T3-8 | 4.842.219 | 6.446.102 | 1228 |
| T3-9 | 4.842.421 | 6.446.874 | 1282 |
| T3-10 | 4.841.856 | 6.446.732 | 1269 |
| T3-11 | 4.841.669 | 6.447.093 | 1300 |
| T3-12 | 4.841.400 | 6.447.361 | 1318 |
| T3-13 | 4.840.950 | 6.447.690 | 1330 |
| T3-14 | 4.840.682 | 6.447.962 | 1340 |
| T3-15 | 4.840.266 | 6.448.045 | 1360 |
| T3-16 | 4.840.169 | 6.448.531 | 1359 |
| T3-17 | 4.839.683 | 6.448.475 | 1341 |
| T3-18 | 4.839.548 | 6.448.930 | 1366 |
| T3-19 | 4.839.030 | 6.449.125 | 1324 |
| T3-20 | 4.838.386 | 6.449.354 | 1339 |
| T3-21 | 4.841.838 | 6.445.312 | 1190 |
| T3-22 | 4.841.505 | 6.445.502 | 1197 |
| T3-23 | 4.841.274 | 6.445.807 | 1230 |
| T3-24 | 4.841.062 | 6.446.217 | 1230 |
| T3-25 | 4.840.658 | 6.446.356 | 1240 |
| T3-26 | 4.840.778 | 6.447.013 | 1298 |
| T3-27 | 4.840.168 | 6.447.102 | 1308 |
| T3-28 | 4.839.757 | 6.447.194 | 1300 |
| T3-29 | 4.839.479 | 6.447.523 | 1308 |
| T3-30 | 4.839.127 | 6.447.717 | 1292 |
| T3-31 | 4.838.950 | 6.448.112 | 1305 |
| T3-32 | 4.838.678 | 6.448.376 | 1289 |
| T3-33 | 4.838.454 | 6.448.873 | 1299 |
| T3-34 | 4.842.060 | 6.444.037 | 1099 |
| T3-35 | 4.841.854 | 6.444.407 | 1158 |
| T3-36 | 4.841.409 | 6.444.427 | 1152 |
| T3-37 | 4.841.176 | 6.444.748 | 1171 |
| T3-38 | 4.840.798 | 6.444.864 | 1154 |
| T3-39 | 4.840.613 | 6.445.302 | 1195 |
| T3-40 | 4.840.351 | 6.445.570 | 1191 |
| T3-41 | 4.840.010 | 6.445.796 | 1178 |
| T3-42 | 4.839.962 | 6.446.301 | 1208 |
| MS3 | 4.841.295 | 6.444.308 | 1160 |

Table 6-3 Energy per turbine

| No. | Gross energy (GWh) | Wake losses (%) | Net energy (GWh) | Capacity factor (%) | Net energy - index (%) |
|-------|--------------------|-----------------|------------------|---------------------|------------------------|
| T2-1 | 5,971 | 4,9 | 5,680 | 28,2 | 82 |
| T2-2 | 5,937 | 3,7 | 5,719 | 28,4 | 83 |
| T2-3 | 6,431 | 5,4 | 6,084 | 30,2 | 88 |
| T2-4 | 6,322 | 4,2 | 6,058 | 30,1 | 88 |
| T2-5 | 5,925 | 2,2 | 5,795 | 28,7 | 84 |
| T2-6 | 6,140 | 8,4 | 5,623 | 27,9 | 81 |
| T2-7 | 5,982 | 7,1 | 5,558 | 27,6 | 80 |
| T2-8 | 5,865 | 5,9 | 5,517 | 27,4 | 80 |
| T2-9 | 5,890 | 6,0 | 5,537 | 27,5 | 80 |
| T2-10 | 6,025 | 4,6 | 5,746 | 28,5 | 83 |
| T2-11 | 6,117 | 5,2 | 5,801 | 28,8 | 84 |
| T2-12 | 6,137 | 4,5 | 5,858 | 29,1 | 85 |
| T2-13 | 6,074 | 5,4 | 5,749 | 28,5 | 83 |
| T2-14 | 6,027 | 5,4 | 5,704 | 28,3 | 82 |
| T2-15 | 6,616 | 5,3 | 6,266 | 31,1 | 91 |
| T2-16 | 6,152 | 4,2 | 5,892 | 29,2 | 85 |
| T2-17 | 6,174 | 4,9 | 5,874 | 29,1 | 85 |
| T2-18 | 6,374 | 3,6 | 6,142 | 30,5 | 89 |
| T2-19 | 6,036 | 2,7 | 5,873 | 29,1 | 85 |
| T2-20 | 6,942 | 0,4 | 6,917 | 34,3 | 100 |
| T2-21 | 6,000 | 10,3 | 5,381 | 26,7 | 78 |
| T2-22 | 6,016 | 6,9 | 5,601 | 27,8 | 81 |
| T2-23 | 6,442 | 6,9 | 6,000 | 29,8 | 87 |
| T2-24 | 6,041 | 8,7 | 5,517 | 27,4 | 80 |
| T2-25 | 6,254 | 5,5 | 5,910 | 29,3 | 85 |
| T2-26 | 6,368 | 6,5 | 5,955 | 29,5 | 86 |
| T2-27 | 6,581 | 7,5 | 6,090 | 30,2 | 88 |
| T2-28 | 6,602 | 5,5 | 6,238 | 30,9 | 90 |
| T2-29 | 6,590 | 7,5 | 6,093 | 30,2 | 88 |
| T2-30 | 6,451 | 3,6 | 6,217 | 30,8 | 90 |
| T2-31 | 6,578 | 5,8 | 6,198 | 30,7 | 90 |
| T2-32 | 6,343 | 2,9 | 6,159 | 30,6 | 89 |
| T2-33 | 6,495 | 3,1 | 6,295 | 31,2 | 91 |
| T2-34 | 5,971 | 4,6 | 5,699 | 28,3 | 82 |
| T2-35 | 6,540 | 6,2 | 6,135 | 30,4 | 89 |
| T2-36 | 6,346 | 5,8 | 5,976 | 29,6 | 86 |
| T2-37 | 6,427 | 8,2 | 5,897 | 29,3 | 85 |
| T2-38 | 6,159 | 4,6 | 5,875 | 29,1 | 85 |
| T2-39 | 6,495 | 6,3 | 6,087 | 30,2 | 88 |
| T2-40 | 6,276 | 8,2 | 5,764 | 28,6 | 83 |
| T2-41 | 5,994 | 4,6 | 5,719 | 28,4 | 83 |
| T2-42 | 6,009 | 4,0 | 5,768 | 28,6 | 83 |
| Avg | 6,241 | 5,4 | 5,904 | 29,3 | 85 |
| Min | 5,865 | 0,4 | 5,381 | 26,7 | 78 |
| Max | 6,942 | 10,3 | 6,917 | 34,3 | 100 |

Table 6-4 Summary data

| | |
|---------------------------------|------------|
| WF Ljubusa | |
| Number of WT | 42 |
| Total net energy (GWh) | 248 |
| Average net energy per WT (GWh) | 5,904 |
| Capacity factor (%) | 29,3 |
| Min/max wake losses (%) | 0,4 - 10,3 |

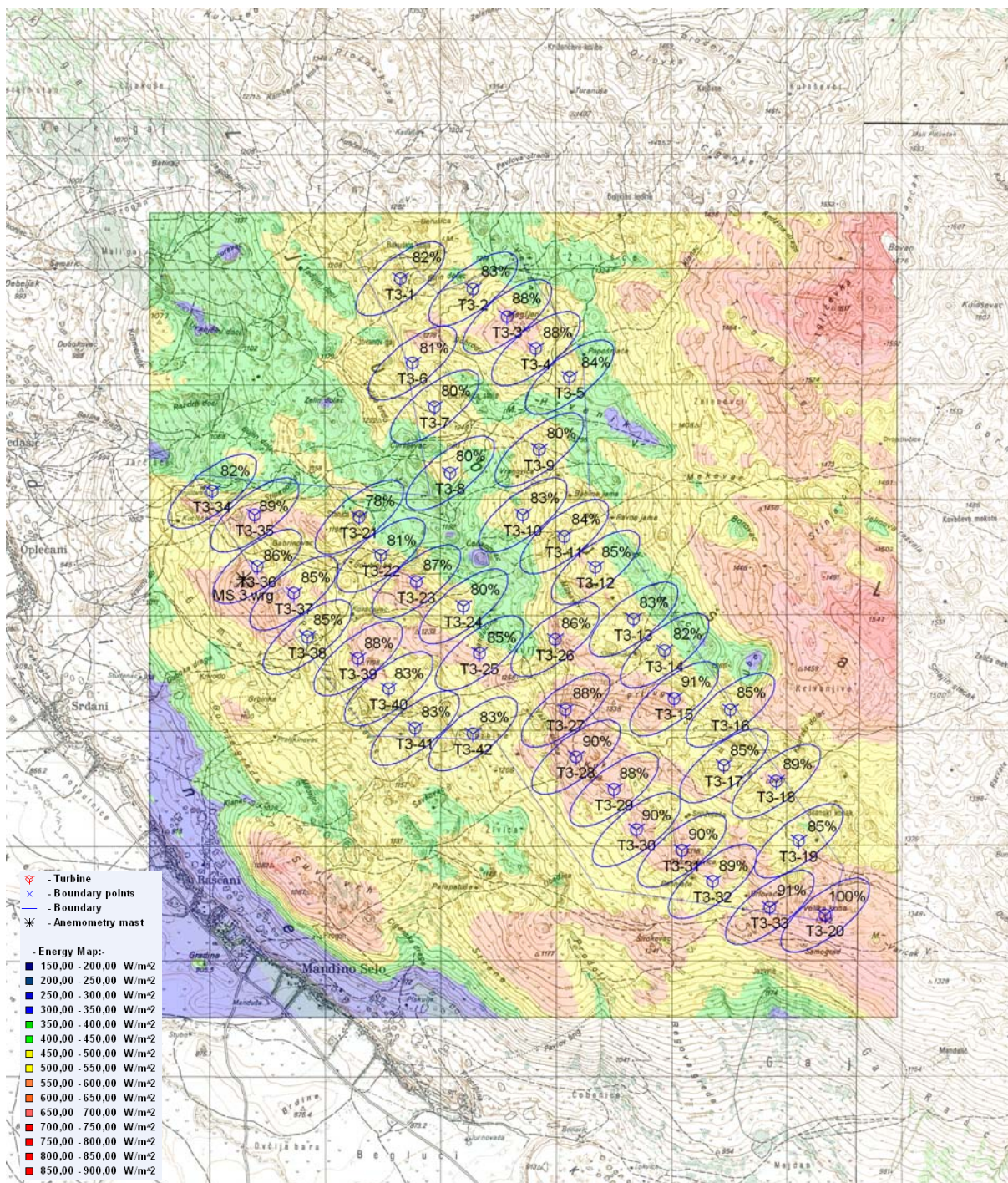


Figure 6-5 Net energy indexes

Table 6-5 Estimated design equivalent turbulence by wind speed (T3-1 – T3-10)

| v(m/s) | T3-1 | T3-2 | T3-3 | T3-4 | T3-5 | T3-6 | T3-7 | T3-8 | T3-9 | T3-10 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,269 | 0,280 | 0,271 | 0,275 | 0,283 | 0,251 | 0,250 | 0,260 | 0,272 | 0,271 |
| 5 | 0,294 | 0,286 | 0,278 | 0,277 | 0,288 | 0,281 | 0,291 | 0,293 | 0,296 | 0,290 |
| 6 | 0,274 | 0,278 | 0,292 | 0,290 | 0,290 | 0,265 | 0,280 | 0,281 | 0,280 | 0,285 |
| 7 | 0,235 | 0,231 | 0,247 | 0,246 | 0,238 | 0,239 | 0,242 | 0,236 | 0,237 | 0,236 |
| 8 | 0,213 | 0,211 | 0,220 | 0,222 | 0,216 | 0,217 | 0,222 | 0,217 | 0,216 | 0,216 |
| 9 | 0,201 | 0,201 | 0,208 | 0,210 | 0,201 | 0,206 | 0,211 | 0,205 | 0,202 | 0,200 |
| 10 | 0,186 | 0,187 | 0,197 | 0,196 | 0,184 | 0,196 | 0,197 | 0,192 | 0,187 | 0,187 |
| 11 | 0,175 | 0,178 | 0,187 | 0,181 | 0,173 | 0,187 | 0,180 | 0,180 | 0,175 | 0,176 |
| 12 | 0,176 | 0,179 | 0,181 | 0,175 | 0,179 | 0,184 | 0,179 | 0,182 | 0,176 | 0,178 |
| 13 | 0,186 | 0,182 | 0,180 | 0,179 | 0,180 | 0,183 | 0,184 | 0,190 | 0,182 | 0,182 |
| 14 | 0,180 | 0,179 | 0,178 | 0,174 | 0,176 | 0,188 | 0,183 | 0,183 | 0,177 | 0,176 |
| 15 | 0,176 | 0,170 | 0,173 | 0,170 | 0,155 | 0,174 | 0,174 | 0,172 | 0,171 | 0,160 |
| 16 | 0,155 | 0,155 | 0,165 | 0,156 | 0,144 | 0,168 | 0,154 | 0,153 | 0,151 | 0,147 |
| 17 | 0,146 | 0,150 | 0,160 | 0,150 | 0,141 | 0,160 | 0,151 | 0,149 | 0,147 | 0,143 |
| 18 | 0,141 | 0,145 | 0,155 | 0,146 | 0,140 | 0,156 | 0,148 | 0,147 | 0,144 | 0,141 |
| 19 | 0,137 | 0,142 | 0,150 | 0,143 | 0,139 | 0,153 | 0,147 | 0,145 | 0,141 | 0,138 |
| 20 | 0,135 | 0,140 | 0,146 | 0,142 | 0,138 | 0,150 | 0,145 | 0,143 | 0,139 | 0,137 |
| 21 | 0,134 | 0,137 | 0,144 | 0,141 | 0,138 | 0,148 | 0,145 | 0,142 | 0,137 | 0,135 |
| 22 | 0,135 | 0,135 | 0,142 | 0,140 | 0,136 | 0,146 | 0,143 | 0,142 | 0,136 | 0,134 |
| 23 | 0,134 | 0,132 | 0,139 | 0,138 | 0,135 | 0,144 | 0,139 | 0,140 | 0,133 | 0,133 |
| 24 | 0,135 | 0,132 | 0,136 | 0,135 | 0,123 | 0,140 | 0,136 | 0,142 | 0,132 | 0,135 |
| 25 | 0,137 | 0,109 | 0,128 | 0,107 | 0,062 | 0,132 | 0,124 | 0,121 | 0,128 | 0,108 |

Table 6-6 Estimated design equivalent turbulence by wind speed (T3-11 – T3-20)

| v(m/s) | T3-11 | T3-12 | T3-13 | T3-14 | T3-15 | T3-16 | T3-17 | T3-18 | T3-19 | T3-20 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,271 | 0,276 | 0,278 | 0,284 | 0,264 | 0,281 | 0,273 | 0,277 | 0,280 | 0,256 |
| 5 | 0,288 | 0,284 | 0,282 | 0,274 | 0,281 | 0,274 | 0,284 | 0,271 | 0,296 | 0,263 |
| 6 | 0,287 | 0,283 | 0,277 | 0,280 | 0,273 | 0,273 | 0,276 | 0,255 | 0,278 | 0,260 |
| 7 | 0,246 | 0,248 | 0,236 | 0,249 | 0,254 | 0,236 | 0,246 | 0,247 | 0,233 | 0,235 |
| 8 | 0,218 | 0,220 | 0,215 | 0,222 | 0,224 | 0,211 | 0,221 | 0,210 | 0,214 | 0,202 |
| 9 | 0,205 | 0,205 | 0,205 | 0,210 | 0,212 | 0,199 | 0,207 | 0,194 | 0,202 | 0,189 |
| 10 | 0,192 | 0,191 | 0,194 | 0,199 | 0,199 | 0,187 | 0,194 | 0,184 | 0,186 | 0,178 |
| 11 | 0,182 | 0,173 | 0,183 | 0,190 | 0,187 | 0,183 | 0,184 | 0,175 | 0,172 | 0,166 |
| 12 | 0,179 | 0,168 | 0,180 | 0,182 | 0,181 | 0,186 | 0,182 | 0,170 | 0,175 | 0,156 |
| 13 | 0,181 | 0,170 | 0,181 | 0,182 | 0,184 | 0,185 | 0,189 | 0,168 | 0,178 | 0,161 |
| 14 | 0,178 | 0,175 | 0,181 | 0,181 | 0,181 | 0,176 | 0,179 | 0,174 | 0,176 | 0,163 |
| 15 | 0,174 | 0,167 | 0,172 | 0,171 | 0,175 | 0,155 | 0,170 | 0,162 | 0,164 | 0,161 |
| 16 | 0,163 | 0,154 | 0,160 | 0,161 | 0,157 | 0,153 | 0,151 | 0,153 | 0,145 | 0,152 |
| 17 | 0,156 | 0,145 | 0,156 | 0,157 | 0,147 | 0,147 | 0,147 | 0,144 | 0,142 | 0,130 |
| 18 | 0,150 | 0,142 | 0,152 | 0,154 | 0,142 | 0,145 | 0,143 | 0,141 | 0,139 | 0,127 |
| 19 | 0,146 | 0,140 | 0,148 | 0,150 | 0,139 | 0,143 | 0,140 | 0,139 | 0,137 | 0,124 |
| 20 | 0,143 | 0,139 | 0,145 | 0,148 | 0,136 | 0,141 | 0,138 | 0,137 | 0,135 | 0,123 |
| 21 | 0,140 | 0,139 | 0,143 | 0,147 | 0,134 | 0,139 | 0,137 | 0,135 | 0,133 | 0,121 |
| 22 | 0,137 | 0,138 | 0,142 | 0,145 | 0,134 | 0,137 | 0,137 | 0,134 | 0,130 | 0,120 |
| 23 | 0,134 | 0,137 | 0,140 | 0,142 | 0,134 | 0,136 | 0,133 | 0,132 | 0,129 | 0,120 |
| 24 | 0,130 | 0,135 | 0,136 | 0,140 | 0,134 | 0,123 | 0,133 | 0,131 | 0,131 | 0,117 |
| 25 | 0,129 | 0,116 | 0,123 | 0,131 | 0,132 | 0,110 | 0,107 | 0,120 | 0,112 | 0,094 |

Table 6-7 Estimated design equivalent turbulence by wind speed (T3-21 – T3-30)

| v(m/s) | T3-21 | T3-22 | T3-23 | T3-24 | T3-25 | T3-26 | T3-27 | T3-28 | T3-29 | T3-30 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,238 | 0,241 | 0,205 | 0,235 | 0,232 | 0,251 | 0,243 | 0,243 | 0,241 | 0,243 |
| 5 | 0,282 | 0,295 | 0,283 | 0,283 | 0,298 | 0,282 | 0,278 | 0,277 | 0,281 | 0,287 |
| 6 | 0,266 | 0,291 | 0,290 | 0,285 | 0,287 | 0,269 | 0,268 | 0,277 | 0,282 | 0,283 |
| 7 | 0,238 | 0,247 | 0,245 | 0,243 | 0,247 | 0,238 | 0,245 | 0,249 | 0,250 | 0,246 |
| 8 | 0,219 | 0,228 | 0,215 | 0,221 | 0,228 | 0,214 | 0,217 | 0,223 | 0,222 | 0,223 |
| 9 | 0,211 | 0,216 | 0,202 | 0,209 | 0,216 | 0,200 | 0,204 | 0,208 | 0,209 | 0,210 |
| 10 | 0,201 | 0,199 | 0,188 | 0,197 | 0,200 | 0,191 | 0,195 | 0,197 | 0,199 | 0,200 |
| 11 | 0,195 | 0,179 | 0,175 | 0,192 | 0,187 | 0,180 | 0,185 | 0,185 | 0,189 | 0,183 |
| 12 | 0,192 | 0,180 | 0,173 | 0,191 | 0,194 | 0,175 | 0,179 | 0,176 | 0,182 | 0,172 |
| 13 | 0,192 | 0,184 | 0,177 | 0,193 | 0,189 | 0,176 | 0,177 | 0,175 | 0,180 | 0,173 |
| 14 | 0,191 | 0,181 | 0,177 | 0,187 | 0,186 | 0,183 | 0,181 | 0,178 | 0,182 | 0,179 |
| 15 | 0,179 | 0,173 | 0,171 | 0,172 | 0,166 | 0,176 | 0,175 | 0,173 | 0,177 | 0,173 |
| 16 | 0,172 | 0,152 | 0,153 | 0,164 | 0,154 | 0,168 | 0,169 | 0,165 | 0,171 | 0,162 |
| 17 | 0,168 | 0,149 | 0,144 | 0,161 | 0,151 | 0,149 | 0,155 | 0,149 | 0,161 | 0,145 |
| 18 | 0,163 | 0,147 | 0,141 | 0,157 | 0,148 | 0,146 | 0,151 | 0,146 | 0,158 | 0,142 |
| 19 | 0,159 | 0,147 | 0,139 | 0,154 | 0,145 | 0,144 | 0,148 | 0,142 | 0,153 | 0,141 |
| 20 | 0,156 | 0,146 | 0,138 | 0,151 | 0,144 | 0,141 | 0,144 | 0,140 | 0,148 | 0,141 |
| 21 | 0,154 | 0,145 | 0,136 | 0,149 | 0,143 | 0,139 | 0,141 | 0,138 | 0,146 | 0,140 |
| 22 | 0,152 | 0,143 | 0,135 | 0,147 | 0,139 | 0,138 | 0,139 | 0,136 | 0,144 | 0,140 |
| 23 | 0,149 | 0,140 | 0,134 | 0,143 | 0,137 | 0,137 | 0,137 | 0,135 | 0,141 | 0,140 |
| 24 | 0,147 | 0,136 | 0,133 | 0,136 | 0,127 | 0,136 | 0,135 | 0,134 | 0,138 | 0,138 |
| 25 | 0,136 | 0,123 | 0,132 | 0,118 | 0,109 | 0,135 | 0,128 | 0,129 | 0,127 | 0,132 |

Table 6-8 Estimated design equivalent turbulence by wind speed (T3-31 – T3-40)

| v(m/s) | T3-31 | T3-32 | T3-33 | T3-34 | T3-35 | T3-36 | T3-37 | T3-38 | T3-39 | T3-40 |
|--------|-------|-------|-------|-------|-------|-------|-------|-------|-------|-------|
| 4 | 0,256 | 0,262 | 0,265 | 0,271 | 0,239 | 0,250 | 0,236 | 0,256 | 0,235 | 0,240 |
| 5 | 0,278 | 0,282 | 0,285 | 0,277 | 0,271 | 0,284 | 0,284 | 0,293 | 0,279 | 0,288 |
| 6 | 0,272 | 0,291 | 0,288 | 0,274 | 0,275 | 0,278 | 0,285 | 0,289 | 0,277 | 0,294 |
| 7 | 0,254 | 0,247 | 0,240 | 0,224 | 0,248 | 0,248 | 0,253 | 0,246 | 0,248 | 0,251 |
| 8 | 0,220 | 0,221 | 0,217 | 0,205 | 0,214 | 0,222 | 0,224 | 0,227 | 0,220 | 0,227 |
| 9 | 0,205 | 0,209 | 0,208 | 0,194 | 0,200 | 0,207 | 0,212 | 0,214 | 0,207 | 0,216 |
| 10 | 0,195 | 0,195 | 0,194 | 0,181 | 0,189 | 0,195 | 0,200 | 0,200 | 0,196 | 0,202 |
| 11 | 0,183 | 0,180 | 0,183 | 0,174 | 0,180 | 0,183 | 0,190 | 0,184 | 0,186 | 0,190 |
| 12 | 0,180 | 0,177 | 0,184 | 0,179 | 0,176 | 0,180 | 0,188 | 0,184 | 0,182 | 0,188 |
| 13 | 0,178 | 0,181 | 0,194 | 0,184 | 0,177 | 0,178 | 0,188 | 0,187 | 0,181 | 0,189 |
| 14 | 0,181 | 0,181 | 0,183 | 0,177 | 0,179 | 0,184 | 0,188 | 0,182 | 0,183 | 0,187 |
| 15 | 0,175 | 0,173 | 0,179 | 0,159 | 0,172 | 0,173 | 0,180 | 0,169 | 0,176 | 0,180 |
| 16 | 0,165 | 0,150 | 0,154 | 0,147 | 0,163 | 0,160 | 0,165 | 0,152 | 0,166 | 0,165 |
| 17 | 0,155 | 0,146 | 0,148 | 0,143 | 0,150 | 0,150 | 0,161 | 0,148 | 0,158 | 0,162 |
| 18 | 0,152 | 0,143 | 0,142 | 0,140 | 0,147 | 0,146 | 0,157 | 0,145 | 0,154 | 0,158 |
| 19 | 0,148 | 0,142 | 0,139 | 0,138 | 0,144 | 0,142 | 0,154 | 0,143 | 0,150 | 0,154 |
| 20 | 0,145 | 0,141 | 0,137 | 0,136 | 0,141 | 0,139 | 0,151 | 0,142 | 0,146 | 0,152 |
| 21 | 0,142 | 0,140 | 0,136 | 0,135 | 0,139 | 0,138 | 0,148 | 0,142 | 0,144 | 0,150 |
| 22 | 0,141 | 0,140 | 0,137 | 0,134 | 0,137 | 0,137 | 0,147 | 0,141 | 0,142 | 0,149 |
| 23 | 0,139 | 0,139 | 0,133 | 0,134 | 0,135 | 0,136 | 0,145 | 0,138 | 0,140 | 0,146 |
| 24 | 0,137 | 0,137 | 0,128 | 0,131 | 0,132 | 0,134 | 0,142 | 0,136 | 0,138 | 0,142 |
| 25 | 0,135 | 0,126 | 0,118 | 0,078 | 0,130 | 0,134 | 0,138 | 0,109 | 0,136 | 0,137 |

Table 6-9 Estimated design equivalent turbulence by wind speed (T2-41 – T2-42)

| v(m/s) | T3-41 | T3-42 |
|--------|-------|-------|
| 4 | 0,252 | 0,247 |
| 5 | 0,288 | 0,292 |
| 6 | 0,289 | 0,283 |
| 7 | 0,247 | 0,237 |
| 8 | 0,228 | 0,218 |
| 9 | 0,216 | 0,204 |
| 10 | 0,201 | 0,190 |
| 11 | 0,187 | 0,185 |
| 12 | 0,190 | 0,192 |
| 13 | 0,197 | 0,190 |
| 14 | 0,187 | 0,185 |
| 15 | 0,176 | 0,160 |
| 16 | 0,156 | 0,153 |
| 17 | 0,150 | 0,149 |
| 18 | 0,147 | 0,146 |
| 19 | 0,146 | 0,144 |
| 20 | 0,146 | 0,143 |
| 21 | 0,147 | 0,141 |
| 22 | 0,147 | 0,137 |
| 23 | 0,146 | 0,135 |
| 24 | 0,146 | 0,110 |
| 25 | 0,101 | 0,097 |

Table 6-10 Summary turbulence data (15m/s)

| WF Kupres | | |
|-----------|-------------|---------------|
| | WT position | I_{15_eff} |
| Min | 5 | 0,155 |
| Max | 40 | 0,180 |
| Avrg | | 0,171 |

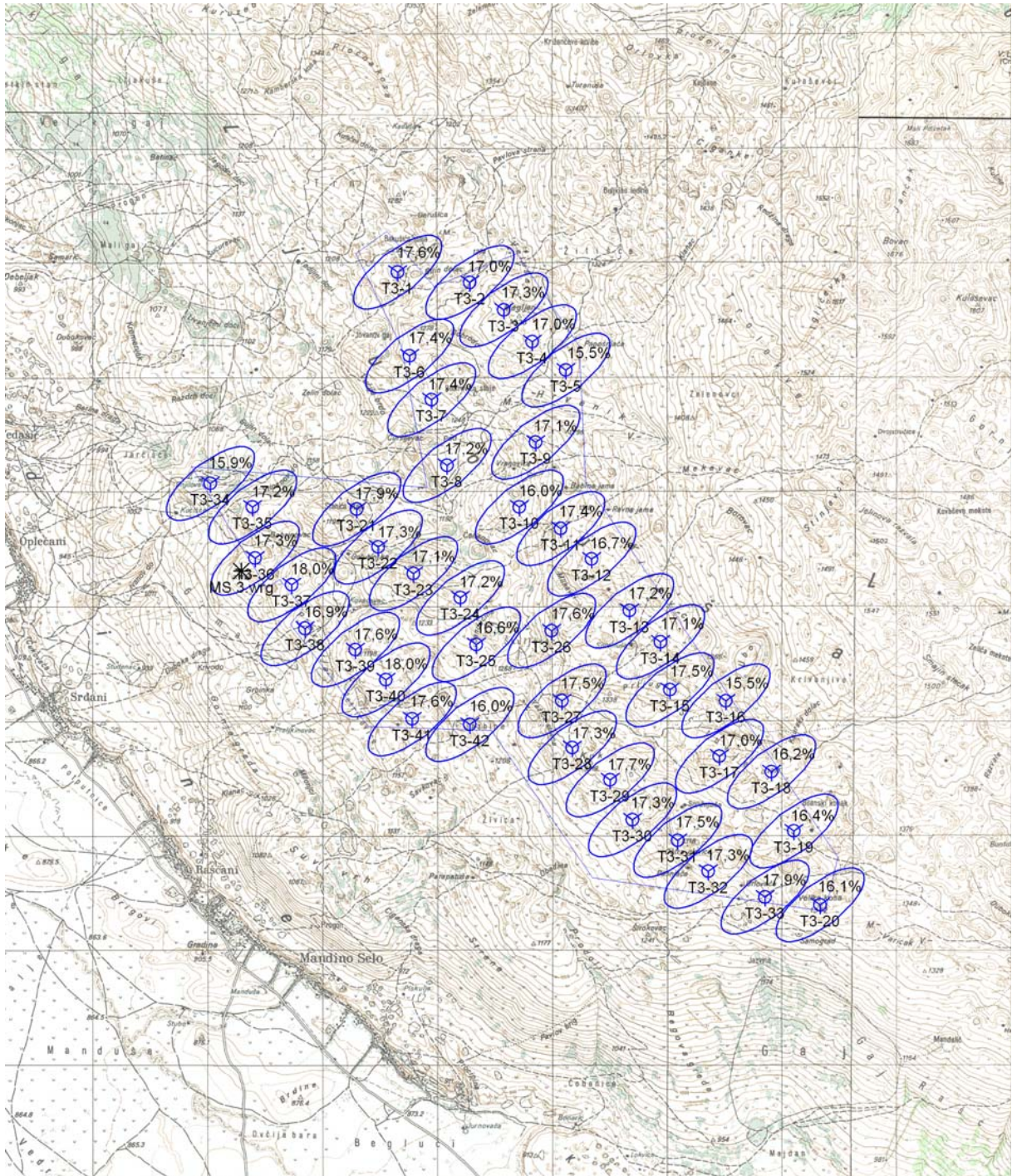


Figure 6-6 Estimated design equivalent turbulence (I_{15_eff}) according to IEC 61400-1 Ed2 standard

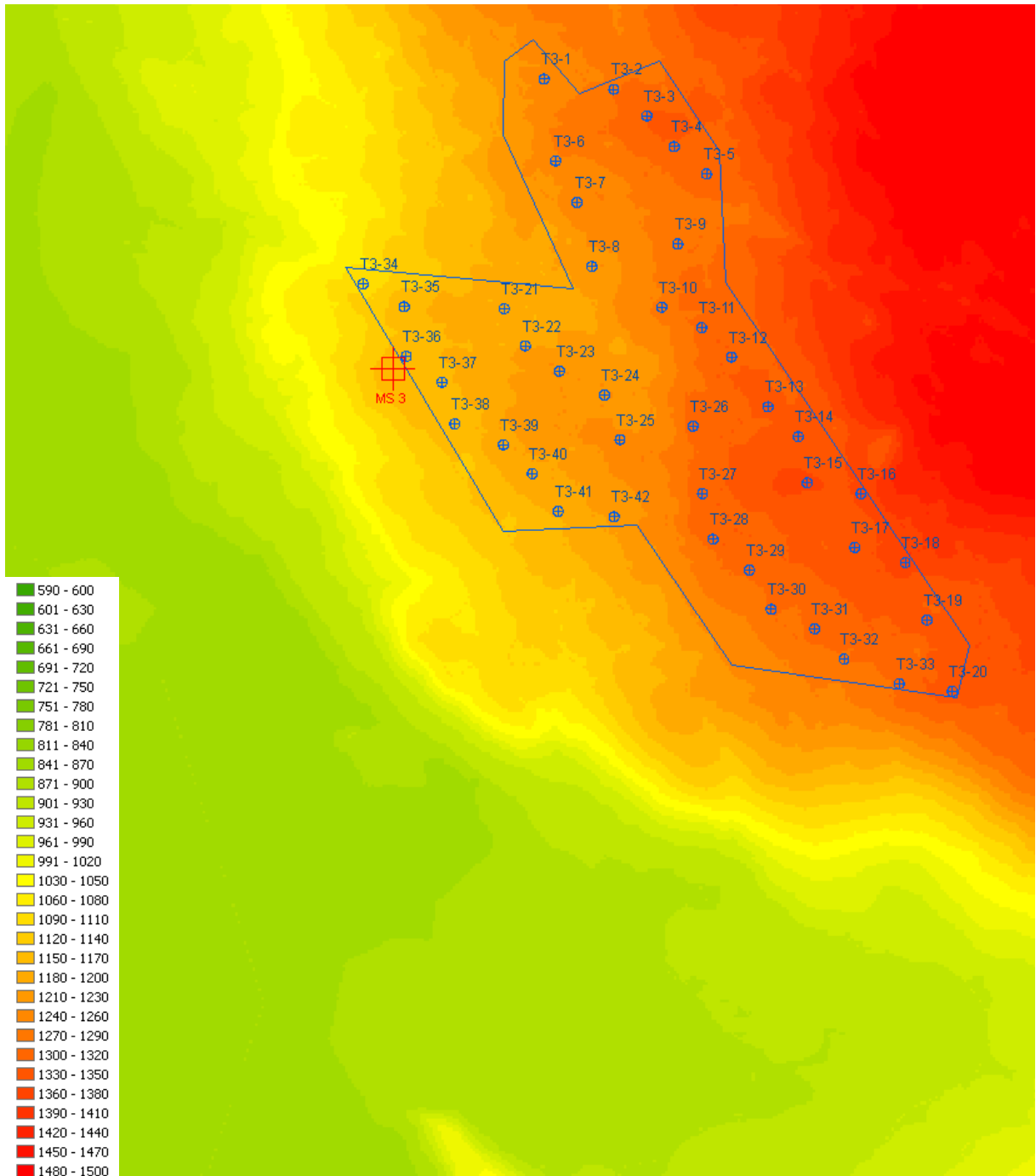


Figure 6-7 Wind turbine positions on height graduated map

7. SUMMARY DATA

Table 7-1 Summary energy report

| WF Kupres | | | WF Pakline | | | WF Ljubusa | | |
|------------|------------|----------|------------|------------|----------|------------|------------|----------|
| No. | Net energy | | No. | Net energy | | No. | Net energy | |
| | (GWh) | c.f. (%) | | (GWh) | c.f. (%) | | (GWh) | c.f. (%) |
| T1-1 | 7,862 | 39,0 | T2-1 | 6,251 | 31,0 | T3-1 | 5,680 | 28,2 |
| T1-2 | 7,142 | 35,4 | T2-2 | 6,283 | 31,2 | T3-2 | 5,719 | 28,4 |
| T1-3 | 5,643 | 28,0 | T2-3 | 6,689 | 33,2 | T3-3 | 6,084 | 30,2 |
| T1-4 | 5,846 | 29,0 | T2-4 | 6,512 | 32,3 | T3-4 | 6,058 | 30,1 |
| T1-5 | 7,452 | 37,0 | T2-5 | 6,530 | 32,4 | T3-5 | 5,795 | 28,7 |
| T1-6 | 7,497 | 37,2 | T2-6 | 6,320 | 31,3 | T3-6 | 5,623 | 27,9 |
| T1-7 | 6,306 | 31,3 | T2-7 | 6,173 | 30,6 | T3-7 | 5,558 | 27,6 |
| T1-8 | 6,172 | 30,6 | T2-8 | 6,432 | 31,9 | T3-8 | 5,517 | 27,4 |
| T1-9 | 7,235 | 35,9 | T2-9 | 6,223 | 30,9 | T3-9 | 5,537 | 27,5 |
| T1-10 | 6,308 | 31,3 | T2-10 | 6,240 | 31,0 | T3-10 | 5,746 | 28,5 |
| T1-11 | 5,696 | 28,3 | T2-11 | 6,244 | 31,0 | T3-11 | 5,801 | 28,8 |
| T1-12 | 6,052 | 30,0 | T2-12 | 6,651 | 33,0 | T3-12 | 5,858 | 29,1 |
| T1-13 | 5,905 | 29,3 | T2-13 | 6,471 | 32,1 | T3-13 | 5,749 | 28,5 |
| T1-14 | 6,036 | 29,9 | T2-14 | 6,570 | 32,6 | T3-14 | 5,704 | 28,3 |
| T1-15 | 6,080 | 30,2 | T2-15 | 6,449 | 32,0 | T3-15 | 6,266 | 31,1 |
| T1-16 | 6,072 | 30,1 | T2-16 | 6,517 | 32,3 | T3-16 | 5,892 | 29,2 |
| T1-17 | 6,231 | 30,9 | T2-17 | 6,100 | 30,3 | T3-17 | 5,874 | 29,1 |
| T1-18 | 6,154 | 30,5 | T2-18 | 6,519 | 32,3 | T3-18 | 6,142 | 30,5 |
| T1-19 | 6,100 | 30,3 | T2-19 | 6,980 | 34,6 | T3-19 | 5,873 | 29,1 |
| T1-20 | 6,417 | 31,8 | T2-20 | 7,339 | 36,4 | T3-20 | 6,917 | 34,3 |
| T1-21 | 6,630 | 32,9 | T2-21 | 7,386 | 36,6 | T3-21 | 5,381 | 26,7 |
| T1-22 | 6,739 | 33,4 | T2-22 | 7,515 | 37,3 | T3-22 | 5,601 | 27,8 |
| T1-23 | 6,071 | 30,1 | T2-23 | 7,612 | 37,8 | T3-23 | 6,000 | 29,8 |
| T1-24 | 5,628 | 27,9 | T2-24 | 7,562 | 37,5 | T3-24 | 5,517 | 27,4 |
| T1-25 | 5,603 | 27,8 | T2-25 | 7,544 | 37,4 | T3-25 | 5,910 | 29,3 |
| T1-26 | 5,789 | 28,7 | T2-26 | 7,807 | 38,7 | T3-26 | 5,955 | 29,5 |
| T1-27 | 5,901 | 29,3 | T2-27 | 7,449 | 37,0 | T3-27 | 6,090 | 30,2 |
| T1-28 | 5,725 | 28,4 | T2-28 | 7,057 | 35,0 | T3-28 | 6,238 | 30,9 |
| T1-29 | 6,240 | 31,0 | T2-29 | 7,566 | 37,5 | T3-29 | 6,093 | 30,2 |
| T1-30 | 6,049 | 30,0 | T2-30 | 7,537 | 37,4 | T3-30 | 6,217 | 30,8 |
| T1-31 | 6,287 | 31,2 | T2-31 | 6,777 | 33,6 | T3-31 | 6,198 | 30,7 |
| T1-32 | 6,630 | 32,9 | T2-32 | 6,624 | 32,9 | T3-32 | 6,159 | 30,6 |
| T1-33 | 7,102 | 35,2 | T2-33 | 6,766 | 33,6 | T3-33 | 6,295 | 31,2 |
| T1-34 | 6,596 | 32,7 | T2-34 | 6,051 | 30,0 | T3-34 | 5,699 | 28,3 |
| T1-35 | 6,385 | 31,7 | T2-35 | 7,176 | 35,6 | T3-35 | 6,135 | 30,4 |
| T1-36 | 6,120 | 30,4 | T2-36 | 7,378 | 36,6 | T3-36 | 5,976 | 29,6 |
| T1-37 | 6,352 | 31,5 | T2-37 | 7,303 | 36,2 | T3-37 | 5,897 | 29,3 |
| T1-38 | 6,524 | 32,4 | T2-38 | 7,216 | 35,8 | T3-38 | 5,875 | 29,1 |
| T1-39 | 6,335 | 31,4 | T2-39 | 7,092 | 35,2 | T3-39 | 6,087 | 30,2 |
| | | | T2-40 | 7,096 | 35,2 | T3-40 | 5,764 | 28,6 |
| | | | T2-41 | 7,060 | 35,0 | T3-41 | 5,719 | 28,4 |
| | | | T2-42 | 6,806 | 33,8 | T3-42 | 5,768 | 28,6 |
| | | | T2-43 | 6,825 | 33,9 | | | |
| | | | T2-44 | 7,118 | 35,3 | | | |
| | | | T2-45 | 7,070 | 35,1 | | | |
| | | | T2-46 | 7,142 | 35,4 | | | |
| | | | T2-47 | 7,182 | 35,6 | | | |
| | | | T2-48 | 6,972 | 34,6 | | | |
| | | | T2-49 | 6,790 | 33,7 | | | |
| | | | T2-50 | 6,588 | 32,7 | | | |
| | | | T2-51 | 6,710 | 33,3 | | | |
| | | | T2-52 | 6,898 | 34,2 | | | |
| | | | T2-53 | 6,525 | 32,4 | | | |
| | | | T2-54 | 6,168 | 30,6 | | | |
| | | | T2-55 | 6,658 | 33,0 | | | |
| Net energy | | | Net energy | | | Net energy | | |
| | (GWh) | c.f. (%) | | (GWh) | c.f. (%) | | (GWh) | c.f. (%) |
| | 247 | 31,4 | | 377 | 34,0 | | 248 | 29,3 |

Table 7-2 Wind turbines sorted by net energy

| No. | Net energy (GWh) | No. | Net energy (GWh) | No. | Net energy (GWh) |
|-------|------------------|-------|------------------|-------|------------------|
| T1-1 | 7,862 | T2-50 | 6,588 | T1-15 | 6,080 |
| T2-26 | 7,807 | T2-14 | 6,570 | T1-16 | 6,072 |
| T2-23 | 7,612 | T2-5 | 6,530 | T1-23 | 6,071 |
| T2-29 | 7,566 | T2-53 | 6,525 | T3-4 | 6,058 |
| T2-24 | 7,562 | T1-38 | 6,524 | T1-12 | 6,052 |
| T2-25 | 7,544 | T2-18 | 6,519 | T2-34 | 6,051 |
| T2-30 | 7,537 | T2-16 | 6,517 | T1-30 | 6,049 |
| T2-22 | 7,515 | T2-4 | 6,512 | T1-14 | 6,036 |
| T1-6 | 7,497 | T2-13 | 6,471 | T3-23 | 6,000 |
| T1-5 | 7,452 | T2-15 | 6,449 | T3-36 | 5,976 |
| T2-27 | 7,449 | T2-8 | 6,432 | T3-26 | 5,955 |
| T2-21 | 7,386 | T1-20 | 6,417 | T3-25 | 5,910 |
| T2-36 | 7,378 | T1-35 | 6,385 | T1-13 | 5,905 |
| T2-20 | 7,339 | T1-37 | 6,352 | T1-27 | 5,901 |
| T2-37 | 7,303 | T1-39 | 6,335 | T3-37 | 5,897 |
| T1-9 | 7,235 | T2-6 | 6,320 | T3-16 | 5,892 |
| T2-38 | 7,216 | T1-10 | 6,308 | T3-38 | 5,875 |
| T2-47 | 7,182 | T1-7 | 6,306 | T3-17 | 5,874 |
| T2-35 | 7,176 | T3-33 | 6,295 | T3-19 | 5,873 |
| T1-2 | 7,142 | T1-31 | 6,287 | T3-12 | 5,858 |
| T2-46 | 7,142 | T2-2 | 6,283 | T1-4 | 5,846 |
| T2-44 | 7,118 | T3-15 | 6,266 | T3-11 | 5,801 |
| T1-33 | 7,102 | T2-1 | 6,251 | T3-5 | 5,795 |
| T2-40 | 7,096 | T2-11 | 6,244 | T1-26 | 5,789 |
| T2-39 | 7,092 | T1-29 | 6,240 | T3-42 | 5,768 |
| T2-45 | 7,070 | T2-10 | 6,240 | T3-40 | 5,764 |
| T2-41 | 7,060 | T3-28 | 6,238 | T3-13 | 5,749 |
| T2-28 | 7,057 | T1-17 | 6,231 | T3-10 | 5,746 |
| T2-19 | 6,980 | T2-9 | 6,223 | T1-28 | 5,725 |
| T2-48 | 6,972 | T3-30 | 6,217 | T3-2 | 5,719 |
| T3-20 | 6,917 | T3-31 | 6,198 | T3-41 | 5,719 |
| T2-52 | 6,898 | T2-7 | 6,173 | T3-14 | 5,704 |
| T2-43 | 6,825 | T1-8 | 6,172 | T3-34 | 5,699 |
| T2-42 | 6,806 | T2-54 | 6,168 | T1-11 | 5,696 |
| T2-49 | 6,790 | T3-32 | 6,159 | T3-1 | 5,680 |
| T2-31 | 6,777 | T1-18 | 6,154 | T1-3 | 5,643 |
| T2-33 | 6,766 | T3-18 | 6,142 | T1-24 | 5,628 |
| T1-22 | 6,739 | T3-35 | 6,135 | T3-6 | 5,623 |
| T2-51 | 6,710 | T1-36 | 6,120 | T1-25 | 5,603 |
| T2-3 | 6,689 | T1-19 | 6,100 | T3-22 | 5,601 |
| T2-55 | 6,658 | T2-17 | 6,100 | T3-7 | 5,558 |
| T2-12 | 6,651 | T3-29 | 6,093 | T3-9 | 5,537 |
| T1-21 | 6,630 | T3-27 | 6,090 | T3-8 | 5,517 |
| T1-32 | 6,630 | T3-39 | 6,087 | T3-24 | 5,517 |
| T2-32 | 6,624 | T3-3 | 6,084 | T3-21 | 5,381 |
| T1-34 | 6,596 | | | | |

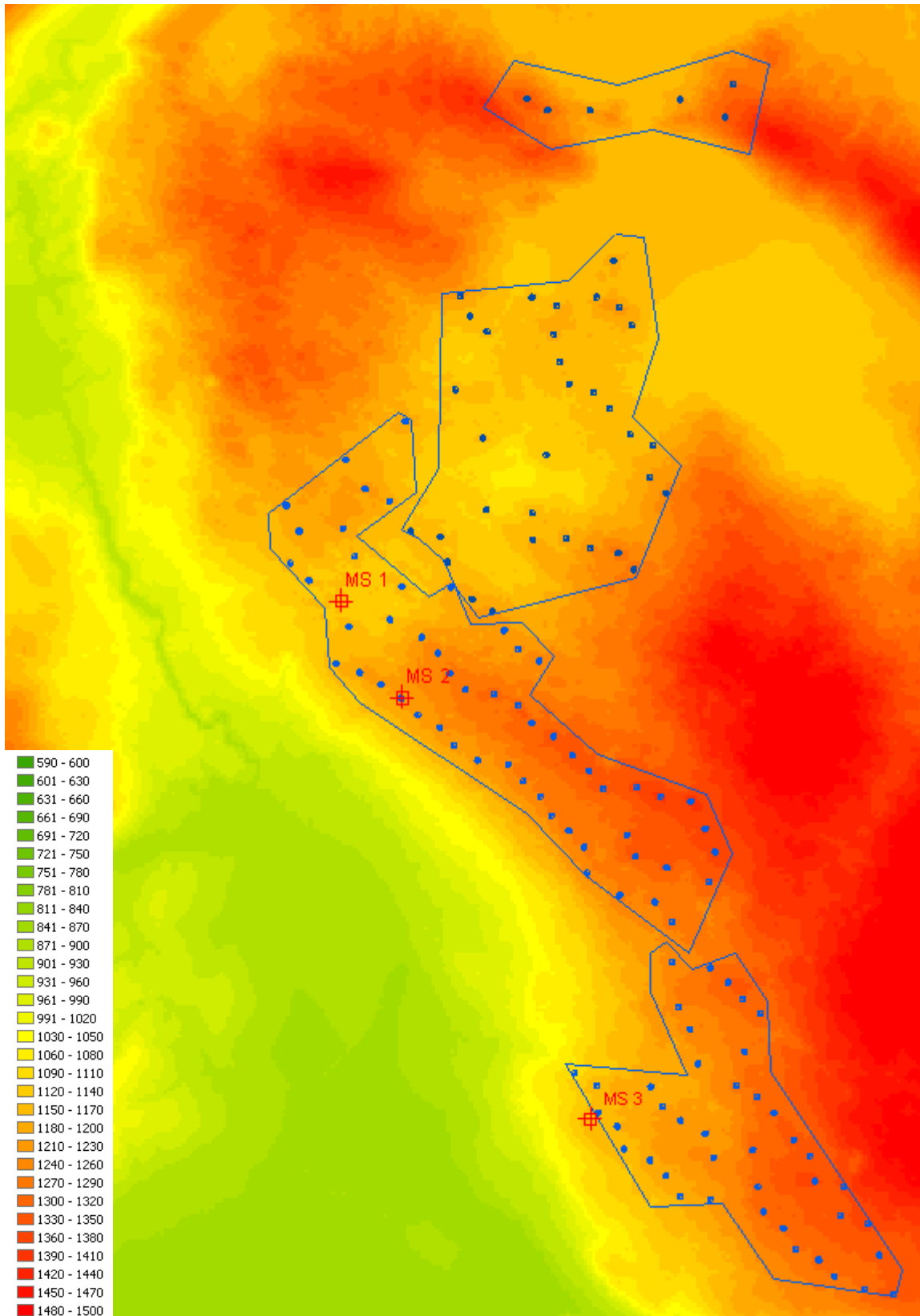


Figure 7-1 Wind turbine positions on height graduated map

APPENDIX - DRAWINGS

1. WF Kupres – wind turbine and measurement mast positions on topography map
2. WF Pakline – wind turbine and measurement mast positions on topography map
3. WF Pakline – wind turbine positions on cadastre map
4. WF Ljubusa – wind turbine and measurement mast positions on topography map
5. WF Ljubusa – wind turbine positions on cadastre map

